

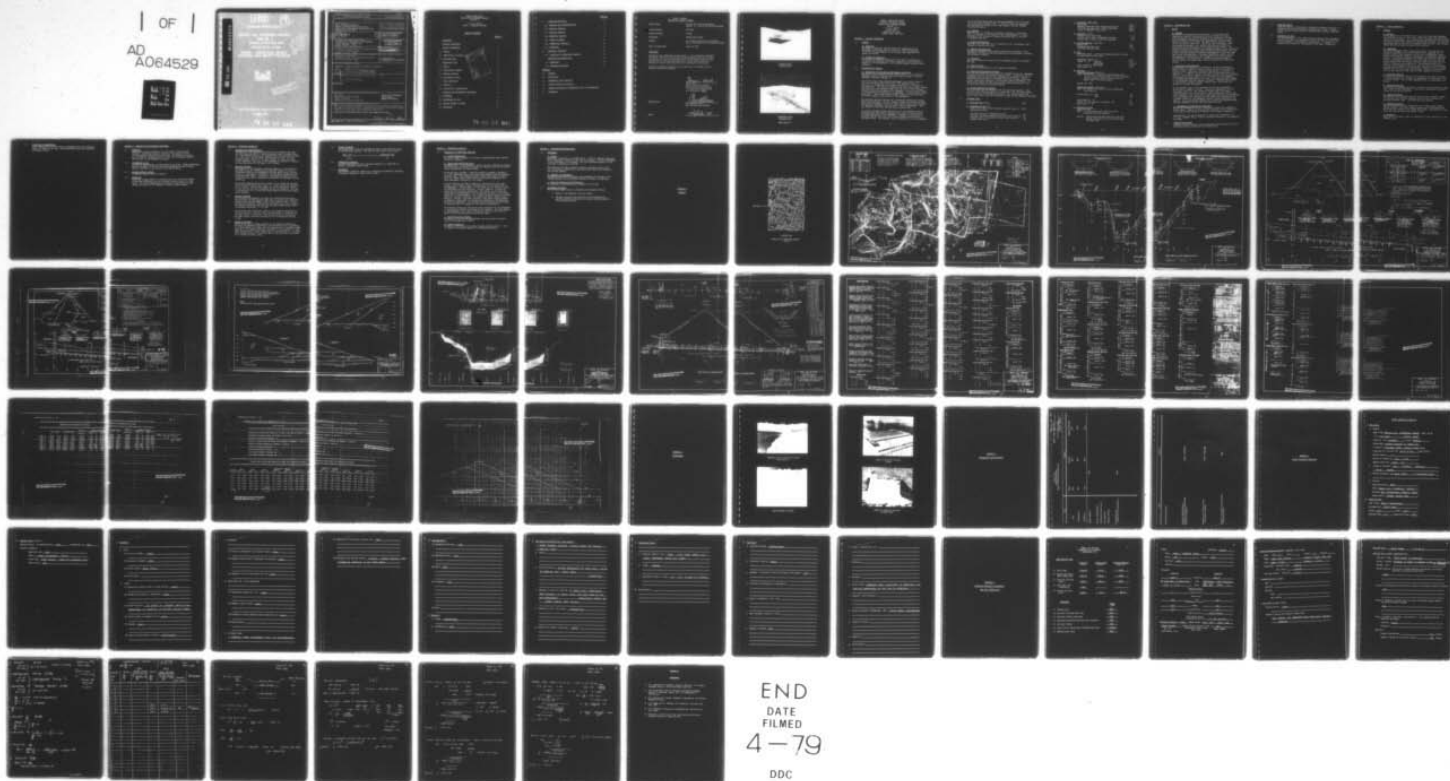
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NEW YORK STATE DEPT OF ENVIRONMENTAL CONSERVATION ALBANY F/G 13/2
NATIONAL DAM SAFETY PROGRAM. BATAVIA KILL WATERSHED PROJECT DAM--ETC(U)
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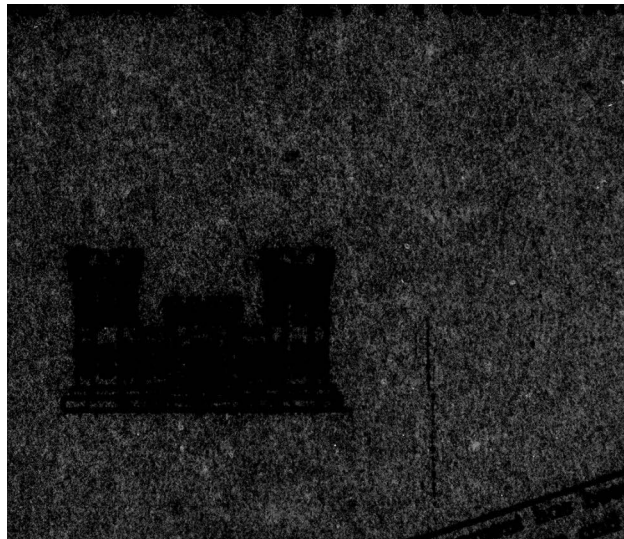
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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report provides information and analysis on the physical condition of the dam as of the report date. Information and analysis are based on visual inspection of the dam by the performing organization. Batavia Kill Watershed Project Dam #3 was judged to be safe.		

MOHAWK RIVER BASIN
BATAVIA KILL WATERSHED PROJECT
DAM No. 3

I.D. No. NY-608
PHASE I INSPECTION REPORT

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PHASE 1 REPORT
NATIONAL DAM SAFETY PROGRAM

Name of Dam: Batavia Kill Watershed Project
Dam No. 3 - I.D. No. NY-608 (#191C-3818)

State Located: New York

County Located: Greene

Watershed: Mohawk River Basin

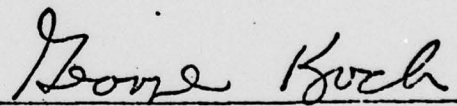
Stream: an unnamed tributary to the Batavia Kill (a tributary to the Schoharie Creek)

Date of Inspection: July 11, 1978

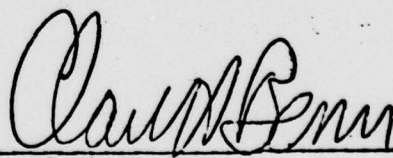
ASSESSMENT

The Batavia Kill Watershed Project Dam No. 3 is a floodwater retarding structure. The earth fill structure was impounding water at the time of inspection to an elevation just above the principal spillway crest. Examination of available documents and a visual inspection of the dam did not reveal conditions which are considered to be unsafe.

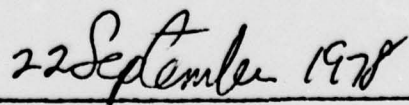
The total discharge capability of the spillways is adequate for the Probable Maximum Flood (PMF).


George Koch
Chief, Dam Safety Section
New York State Department of
Environmental Conservation
N.Y. License No. 45937

Approved by:


Col. Clark H. Benn
New York District Engineer

Date:


22 September 1978



UPSTREAM SLOPE
(looking East)



DOWNSTREAM SLOPE
(looking East)

BKWP DAM No. 3

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
BATAVIA KILL WATERSHED PROJECT
DAM No. 3
I.D. No. NY-608
(#191C-3818)
MOHAWK RIVER BASIN
GREENE COUNTY, NEW YORK

SECTION 1: PROJECT INFORMATION

1.1 GENERAL

a. Authority

The Phase I Inspection reported herein was authorized by the Department of the Army, New York District, Corps of Engineers, to fulfill the requirements of the National Dam Inspection Act, Public Law 92-367.

b. Purpose of Inspection

To evaluate the existing conditions of the dam, to identify deficiencies and hazardous conditions, determine if they constitute hazards to life and property, and recommend remedial measures where necessary.

1.2 DESCRIPTION OF PROJECT

a. Description of the Dam and Appurtenant Structures

The Batavia Kill Watershed Project (BKWP) Dam No. 3 is an earthfill embankment having a principal spillway passing through it and two emergency spillways flanking it.

The 63 foot high, zoned compacted embankment has a crest length of 1100 feet and crest width of 20 feet. The upstream slope is 1 vertical on 3 horizontal and the downstream slope is 1 vertical on 2.5 horizontal. The crest and exposed slopes are heavily grass covered. That portion of the upstream slope below the level of the principal spillway crest did not appear to be ripped. An earth cutoff trench of varying depth and width keys the embankment to the underlying foundation soils. Rock-lined channels extend outward on each side from the outlet channel, along the toe of the embankment.

The principal spillway consists of a rectangular reinforced concrete drop inlet structure, a 30 inch diameter reinforced concrete pressure pipe with anti-seepage collars, an impact basin, and an outlet channel. Two emergency spillways, one each side, flank the embankment. Both are located in earth cuts and are heavily grass-lined.

An internal drainage system consisting of 10 inch diameter fully bituminous coated perforated corrugated metal pipe is located beneath the downstream slope of the embankment. Seepage is collected and conducted through this drain and outleted through the side walls of the impact basin. The reservoir drain consisting of a 16 inch diameter

cast iron pipe extends from the upstream embankment toe to the base of the principal spillway riser. A vertical slide gate mechanism mounted along the inside of the riser controls the flow through the reservoir drain.

b. Location

BKWP Dam No. 3 is located on an unnamed tributary to the Batavia Kill, a tributary to the Schoharie Creek, approximately 1.5 miles Northeast of the village of Windham along Nauvo Road in the Town of Windham, New York.

c. Size Classification

This dam is 63 feet high and is classified as an "intermediate" dam (between 40 and 100 feet high).

d. Hazard Classification

The dam is classified "high" hazard because of the presence of approximately 60 homes and multiple-dwelling units downstream, including the village of Windham.

e. Ownership

This dam is owned by the Batavia Kill Watershed District of Windham, New York.

f. Purpose of Dam

The dam's primary purpose is for retarding floodwaters.

g. Design and Construction History

This dam and appurtenant structures were designed by the U.S. Department of Agriculture, Soil Conservation Service (SCS). Construction of the embankment began in 1970 and was completed the same year. The SCS office having jurisdiction for Greene County has a design folder containing hydrologic, hydraulic, and structural design information, the design calculations for modifications made during construction, and the as-built contract plans and documents.

h. Normal Operating Procedures

Water releases from the reservoir over the principal spillway. This structure has sufficient capacity to discharge a 100 year flood without flow occurring in the emergency spillways. For storms greater than the 100 year flood, flow will discharge through the two emergency spillways.

1.3

PERTINENT DATA

a. Drainage Area (acres)

2304

b. Discharge at Dam (cfs)

Total (of all facilities excluding reservoir drain) @ 17600
Maximum High Water

Principal Spillway @ Maximum High Water	132
Principal Spillway @ Emergency Spillway Crest Elevation	125
Reservoir Drain @ Principal Spillway Crest Elevation	28
Maximum Known Flood	90

c. Elevation (USGS datum)

Top of Dam	1746.9
Emergency Spillway Crest (Auxiliary Spillway)	1739.7
Principal Spillway Crest (Service Spillway)	1699.7
Invert of Reservoir Drain Inlet	1685.5

d. Reservoir (acres)

Surface area @ Top of Dam	71.0
Surface area @ Crest of Emergency Spillway	54.3
Surface area @ Crest of Principal Spillway	4.6

e. Storage Capacity (acre-feet)

Top of Dam	1415
Emergency Spillway Crest	975
Principal Spillway Crest	23.0

f. Dam

Embankment type: a two-zoned compacted earth fill with an earth keyed cutoff trench.

Embankment length (ft)	1100
Slopes (V : H) Upstream	1 on 3
Downstream	1 on 2.5
Crest elevation (USGS datum)	1746.9
Crest width (ft)	20

g. Spillway

Principal Spillway (Service):

Type: Uncontrolled, reinforced concrete drop inlet (2.5 x 7.5 ft) rising 18 feet; 30 inch reinforced concrete pressure conduit 326 feet long; an impact basin; an outlet channel.

Length (ft): Weir	15.0
-------------------	------

Emergency Spillway (Auxiliary):

Type: Two grass-lined channels having trapezoidal cross sections

Bottom Width (ft): East	50
West	200
Side Slopes (V : H)	1:3
Length of level section (in profile) (ft)	50
Exit Slope (V : H)	1:32

h. Regulating Outlet

Reservoir Drain:

Type: 16 inch diameter cast iron pipe with a reinforced concrete headwall.

Control: Mechanically-operated vertical slide gate mounted along the inside of the principal spillway riser.

SECTION 2: ENGINEERING DATA

2.1 DESIGN

a. Geology

The Batavia Kill Watershed Project Dam No. 3 is located in the "Appalachian Uplands" physiographic province of New York State. These uplands are the northern extreme of the Appalachian Plateau and were formed by dissection of the uplifted but flat-lying sandstones and shales of the Middle and Upper Devonian Catskill Delta (395 to 345 million years ago). Relief is high to moderate. Maximum dissection occurs in the Catskill Mountain area where only the mountain peaks approximate the original plateau surface. The present surficial soil deposits have resulted primarily from glaciations during the Cenozoic Era (most recent 65 million year period), the last of which was the Wisconsin glaciation approximately 11,000 years ago. These soils were deposited, in general, directly by glacier ice and are composed of unstratified rock fragments of all sizes ranging from boulders to clay particles. Locally intercalated lenses of sand and gravel are common where ice-laid and water-laid deposition occurs.

b. Subsurface Investigations

A subsurface investigation was conducted by the Soil Conservation Service, with Mr. Ronald C. Page in charge, in the Fall of 1967 and Winter of 1968. Applicable subsurface information is included in Appendix A. In general the surficial soils at the project site consist of a thin layer of topsoil and recent alluvium over sand and gravel outwash and ice contact deposits over glacial till, over sandstone to a maximum explored depth of 61.0 feet. Only boring DH #352 located in the principal spillway extended to bedrock. Observed water levels in the borings is highly variable, ranging from 1 foot below the surface to no water encountered.

An intercalated lense of very permeable gravel was encountered in boring #54 at a depth of 25 feet. Concern was expressed by the review agent (NYS D.O.T. Soil Mechanics Bureau) that this gravel, encountered below the cut-off trench, would promote the flow of subsurface seepage if not controlled. Additional subsurface investigations were progressed which indicated that the gravel was discontinuous and a natural blanket of less permeable material existed upstream of the deposit. As a precautionary measure the toe drain was extended toward the left abutment to collect any flow from this area.

c. Embankment and Appurtenant Structures

The dam was designed by the Soil Conservation Service who prepared a design report. Twenty two drawings were prepared for the construction of the dam of which portions of several are included in Appendix A.

Hydraulically, the dam was designed to retard the floodwaters of a 100 year frequency storm, without a discharge occurring in the emergency spillways.

2.2 CONSTRUCTION RECORDS

Complete as-built contract plans and documents were available from the SCS office having jurisdiction for Greene County.

2.3

OPERATION RECORD

Since the dam is an uncontrolled, floodwater retarding structure, no operating records are maintained regarding water levels. However, during periods of heavy rainfall, SCS personnel do monitor reservoir levels.

2.4

EVALUATION OF DATA

The data presented in this report has been compiled from information obtained from the Soil Conservation Service as well as the New York State Department of Environmental Conservation. It appears to be adequate and reliable for the purpose of the Phase 1 inspection.

SECTION 3: VISUAL INSPECTION

3.1 FINDINGS

a. General

Visual inspection of the BKWP Dam No. 3 and the surrounding watershed was conducted on July 11, 1978. The weather was clear and temperatures ranged in the seventies. The inspection was conducted during a basically dry period during which occasional thunderstorms occurred. The dam was impounding water at the time of inspection with the water level slightly higher than the principal spillway crest elevation.

b. Embankment

The earth embankment shows no signs of distress. The vertical and horizontal alignment of the crest appears to be unchanged, with no visible surface cracks appearing on the crest or embankment slopes. There was no apparent sloughing, subsidence, or depressions occurring either. No noticeable seepage on the downstream slope was observed. However, discharges estimated at less than 5 gpm per outlet were observed flowing from the internal drainage system indicating that the system is functioning satisfactorily. The upstream slope did not have any visible riprap placed at or near the level of the principal spillway crest elevation. No undesirable vegetative growth or animal penetrations into the slopes were observed. However, the heavy grass cover on the slopes was high, making visual inspection difficult.

c. Principal Spillway

The principal spillway consists of the vertical drop inlet structure, a concrete pressure pipe through the embankment, an impact basin, and an outlet channel. All of these components were in satisfactory condition.

d. Emergency Spillway

Two grass-lined emergency spillways, one each side and located in earth cuts, flank the main embankment. Both were in satisfactory condition except for the need for mowing.

e. Regulating Outlet

The reservoir drain conduit and slide gate are the components capable of regulating the reservoir whenever the pool level is below the principal spillway crest. The slide gate does operate.

f. Downstream Channel

The outlet channel quickly transitions into a steep sided V-shaped natural channel. The outlet channel riprap was in satisfactory condition but the V-channel side slopes were eroded. Some debris and logs were also scattered along the channel invert.

g. Reservoir

There was no noticeable signs of landslides or soil instability in the reservoir area.

3.2

EVALUATION OF OBSERVATIONS

Visual observations did not reveal any problems which would adversely affect the safety of the dam. Minor deficiencies may be corrected by maintenance efforts.

SECTION 4: OPERATION AND MAINTENANCE PROCEDURES

4.1 PROCEDURE

Normal water surface elevation is at the crest of the principal spillway. Downstream flows are limited by the capacity of the 30 inch diameter reinforced concrete pipe. The reservoir provides 952 acre-feet of storage between the crest of the principal spillway and the crest of the emergency spillways.

4.2 MAINTENANCE OF DAM

The dam and appurtenances are maintained by the owner. Normal maintenance consists primarily of mowing the grassed emergency spillway bottoms, which at the time of the inspection had been deferred.

4.3 WARNING SYSTEM IN EFFECT

No apparent warning system is present.

4.4 EVALUATION

Sufficient storage capacity is provided such that controlled release of impounded floodwaters by the principal spillway occurs in a safe manner. The dam and appurtenant structures are satisfactorily maintained with mowing of the emergency spillway bottoms required.

SECTION 5: HYDROLOGIC/HYDRAULIC

5.1 DRAINAGE AREA CHARACTERISTICS

Delineation of the watershed draining into the reservoir pool area was made using the USGS 7.5 minute quadrangle sheet for Hensonville, N.Y. The watershed consists of grassed fields and woodlands situated in a rural area. Relief ranges from moderate to steep, with the steeper slopes occurring in the upper reaches and along the sides of the watershed. The slope of the watershed is generally triangular with the dam located at the apex of the triangle.

5.2 ANALYSIS CRITERIA

The analysis of the floodwater retarding capability of this dam was performed using the "Dimensionless Hydrograph" method of the Soil Conservation Service and recommended spillway design flood criteria of the U.S. Army Corps of Engineers. The SCS method establishes the hydrograph peak inflow. A short-cut, approximation method of flood routing was then used to determine the reservoir storage/peak outflow conditions.

The Probable Maximum Flood 6-hour rainfall of 23 inches was selected using the Weather Bureau TP-40 (Ref. 1). Direct runoff was estimated at 20.3 inches. An SCS curve number (CN) of 80 was used to account for the soil and land use development within the watershed. The time of concentration of 1.32 hours was taken directly from the SCS design report summary.

5.3 SPILLWAY CAPACITY

The principal and emergency spillways are uncontrolled structures. The principal spillway operates under weir or orifice flow conditions depending upon the floodwater inflow to the reservoir pool. During orifice flow operation, pressure flow develops in the 30 inch conduit. The emergency spillways were analyzed as broad-crested weirs having a discharge coefficient, C , of 3.087.

The spillways have sufficient capacity for discharging the peak outflow from the PMF. For this storm, the peak inflow is 18500 cfs and the peak outflow is 15900 cfs. When the spillways are discharging the peak outflow, the water surface will be 0.5 feet below the top of dam.

5.4 RESERVOIR CAPACITY

Normal flood control storage capacity of the reservoir between the principal and emergency spillways is 952 acre-feet which is equivalent to a runoff depth of 5 inches over the drainage area. Surge storage capacity to the maximum high water elevation is an additional 440 acre-feet; equivalent to a runoff depth over the drainage area of 2.3 inches. Total storage capacity of the entire dam is 1415 acre-feet; equivalent to 7.4 inches of direct runoff.

5.5

FLOODS OF RECORD

The maximum known flood was reported as being 10 feet above the crest of the principal spillway. The data for this flood is as follows:

<u>Elev. (Ft.)</u>	<u>Discharge (cfs)</u>
1709.7	90

5.6

OVERTOPPING POTENTIAL

Analysis indicates the total discharge capability is sufficient to prevent overtopping from the PMF.

5.7

EVALUATION

This dam has sufficient capability to impound and adequately discharge floodwaters expected to result from the PMF.

SECTION 6: STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. Visual Observations

No signs of major distress of the dam and appurtenances were observed during the inspection.

b. Design and Construction Data

The BKWP Dam No. 3 was designed in 1968 by the Soil Conservation Service. The design data and as-built drawings are available from the SCS office having jurisdiction for Greene County.

The design data included a stability analysis, included in Appendix A, of the downstream slope with steady state seepage from the emergency spillway crest. The minimum factor of safety under these conditions was 1.75. There were no other stability analyses performed on the earth embankment, spillways or cut slopes.

As-built drawings included in Appendix A indicated that there was a change in the location, extent and composition of the three zones in the embankment. Revised sheet 7 of 22, dated 1/27/71, shows the zones and materials that were specified. As-built sheet No. 27 shows the zones that were actually constructed. The changes in the zones are insignificant except possibly for the reduction in Zone 3 at the downstream toe of the embankment. This change reduced the amount of seepage water that the zone 3 material can collect and remove from the zone 2 material. However, this hasn't created a significant problem because no seepage or other signs of distress were observed on the downstream slope of the embankment. The internal drainage system was constructed as specified and it is apparently functioning satisfactorily.

The available design and construction data indicates that the embankment is stable and no further investigations are required. The zone changes in the embankment do not have a significant effect on the stability analysis which was performed during design stages.

c. Post-Construction Changes

No changes to the dam and appurtenances that would cause structural stability problems have occurred.

d. Seismic Stability

The dam is located near the boundary between seismic zones No. 1 and 2; therefore, no seismic analysis is considered warranted.

SECTION 7: ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety

The Phase 1 inspection of the BKWP Dam No. 3 did not indicate conditions which constitute a hazard to human life or property. The earth embankment is not considered to be unstable. The total discharge capacity of the spillways is adequate for the PMF.

The design of this dam includes an internal drainage system to control the phreatic surface and to provide a safe outlet for foundation and internal seepage.

b. Adequacy of Information

Information concerning the design and performance of this dam is considered adequate for the purposes required for Phase 1 inspections.

c. Need for Additional Investigations

No additional investigations are necessary at this time.

7.2 RECOMMENDED MEASURES

The following tasks should be undertaken by maintenance forces:

- a. Mowing of the emergency spillway inverts.
- b. Periodic operation and lubrication of the mechanically-operated slide gate mechanism to insure continued operation of the reservoir drain.

APPENDIX A

DRAWINGS

DAM SITE



VICINITY MAP

BATAVIA KILL WATERSHED PROJECT
DAM No. 3

LAYOUT DATA CURVE 1

Δ: 10° 55' T: 307.76
R: 231 E: 146.13
D: 22° 50' H: 92.36
L: 445

E. STATION	DEFLECTION	CORD DIST.
5+50	0° 00'	49.93
5+00	5° 42'	
4+50	11° 25'	
4+00	17° 08'	
3+50	22° 50'	
3+00	28° 32'	
2+50	34° 15'	
2+00	39° 58'	
1+50	45° 40'	
1+05	50° 48'	44.94

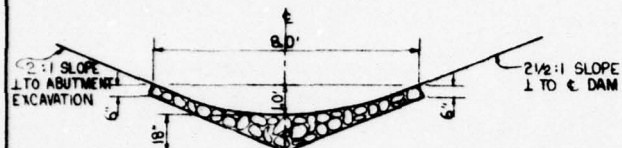
STONE GUTTER CONSTRUCTION DETAILS

CONSTRUCT OF OVERSIZE ROCK FROM THE EMERGENCY SPILLWAYS AND BORROW AREA. ROCK TO BE WELL GRADED WITH A MAXIMUM SIZE OF 18". LOCATION TO BE ALONG INTERFACE BETWEEN DOWN-STREAM SLOPE OF DAM AND THE ABUTMENT EXCAVATION.

ABUTMENT AND FOUNDATION EXCAVATION DETAILS

ABUTMENT EXCAVATION-SLOPE LEFT ABUTMENT TO 2:1 SLOPE, SEE SHEET 4. SLOPE EXCAVATION LIMITS 290' UPSTREAM AND 180' DOWNSTREAM FROM C.O. DAM

FOUNDATION EXCAVATION-EXCAVATE THE "J" MATERIAL FROM THE BASE WIDTH OF THE DAM IN THE FLOOD PLAIN UPSTREAM FROM THE CUTOFF TRENCH SEE SHEETS 4 AND 19 FOR DESCRIPTION OF MATERIAL "J"



TYPICAL SECTION OF STONE GUTTER
Not to Scale

BENCH MARK DESCRIPTION

BM #4 ELEV 1716.15 CHISELED CROSS
PAINTED RED 14" ABOVE GROUND ON
LARGE ROCK



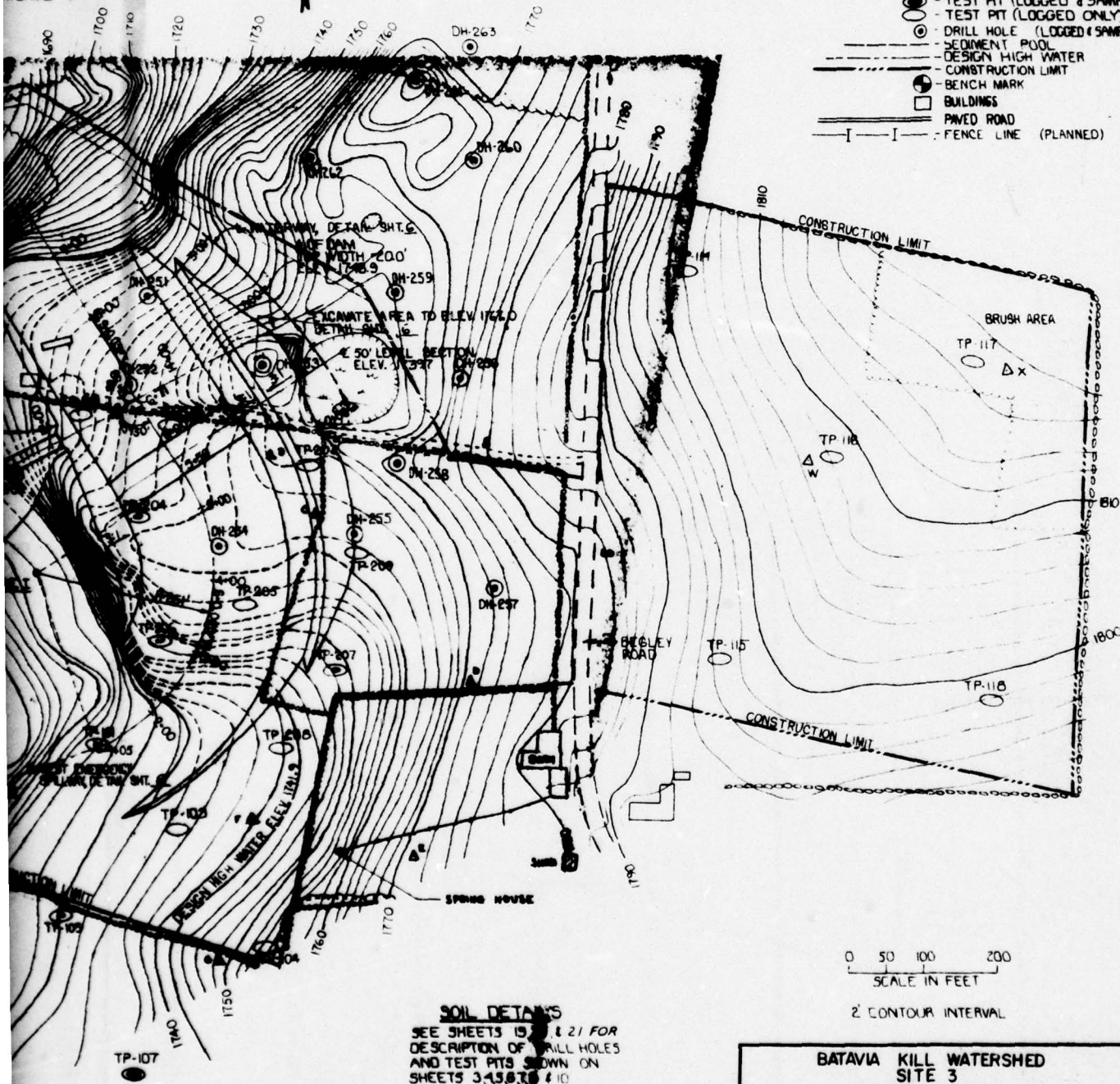
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EXCAVATE THE "J" MATERIAL
OF THE DAM IN THE FLOOD PLAIN
OFF TRENCH SEE SHEETS 4 AND
MATERIAL "J"

$\Delta = 19.45$ $T = 50.53$
 $R = 290$ $E = 4.37$
 $D = 19.45$ $M = 4.30$
 $L = 100$

STATION	DEFLECTION	CORD DIST.
4+04	0'00	0.00
4+29	2'28	24.99
4+54	4'56	24.99
4+79	7'25	24.99
5+04	9'53	24.99

- STONE WALL
- FENCE LINE (EXISTING)
- WOODED AREA
- TRAVERSE HUB
- CENTER LINE OF STREAM
- DIRT ROAD
- POWER LINE
- TEST PIT (LOGGED & SAMPLED)
- TEST PIT (LOGGED ONLY)
- DRILL HOLE (LOGGED & SAMPLED)
- SEDIMENT POOL
- DESIGN HIGH WATER
- CONSTRUCTION LIMIT
- BENCH MARK
- BUILDINGS
- PAVED ROAD
- FENCE LINE (PLANNED)



SOIL DETAILS
SEE SHEETS 19 & 21 FOR
DESCRIPTION OF SOIL HOLES
AND TEST PITS SHOWN ON
SHEETS 34, 37 & 40

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BATAVIA KILL WATERSHED
SITE 3

FLOODWATER RETARDING DAM

PLAN OF STRUCTURAL WORKS

**U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE**

Dr. J. E. POLULECH

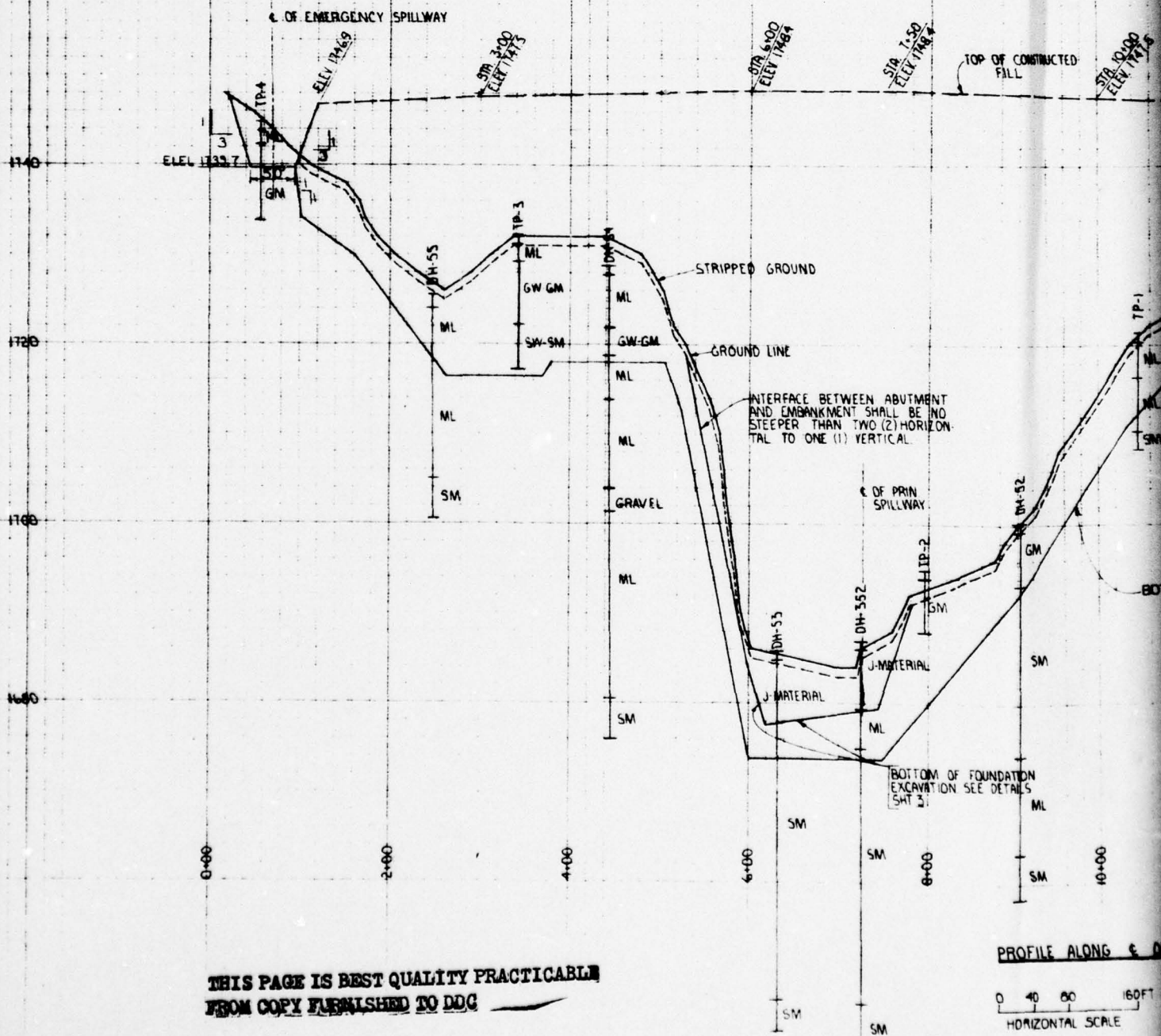
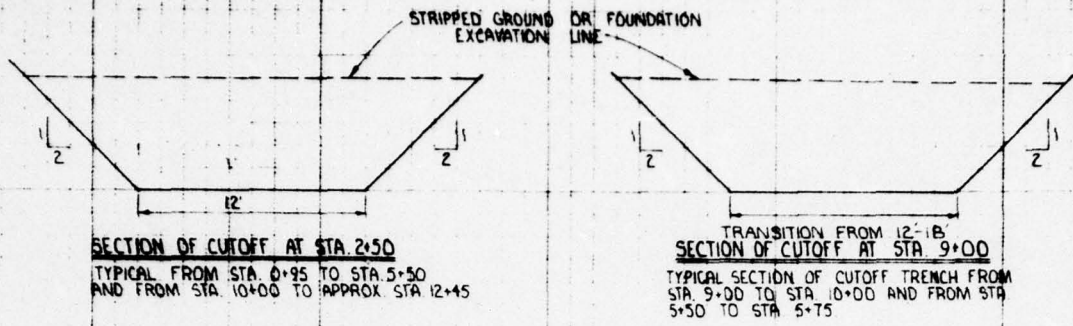
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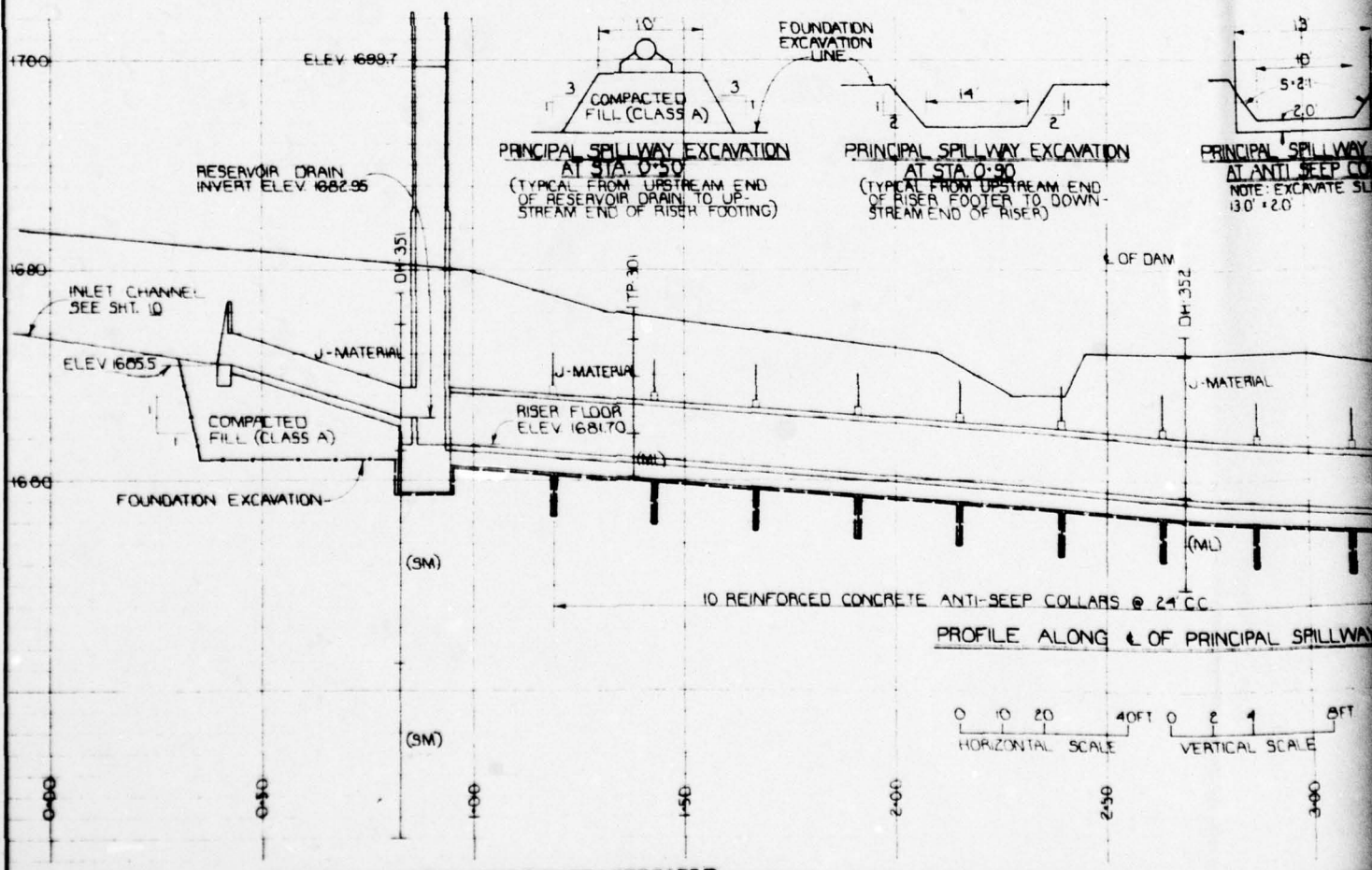
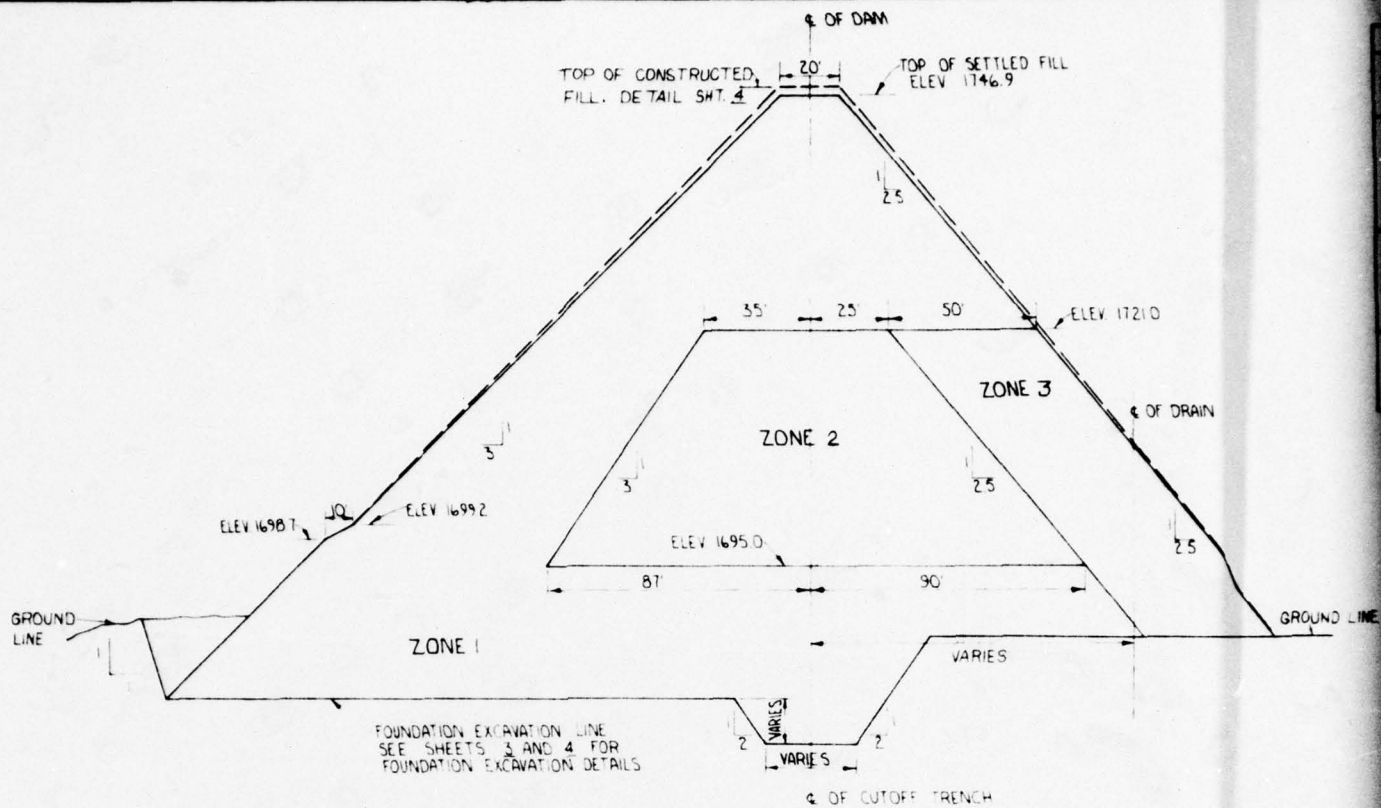
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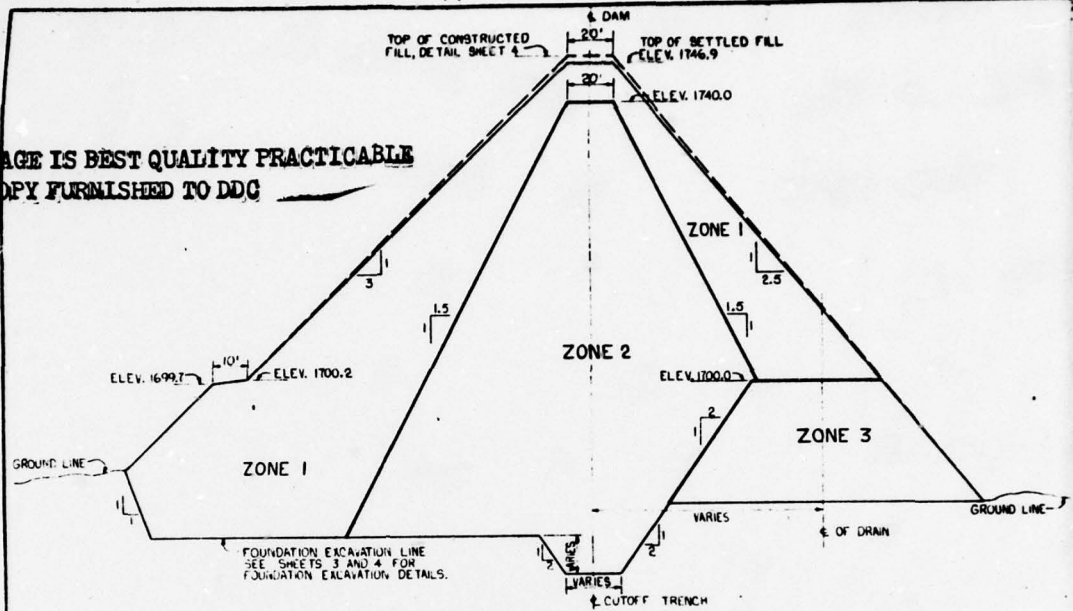


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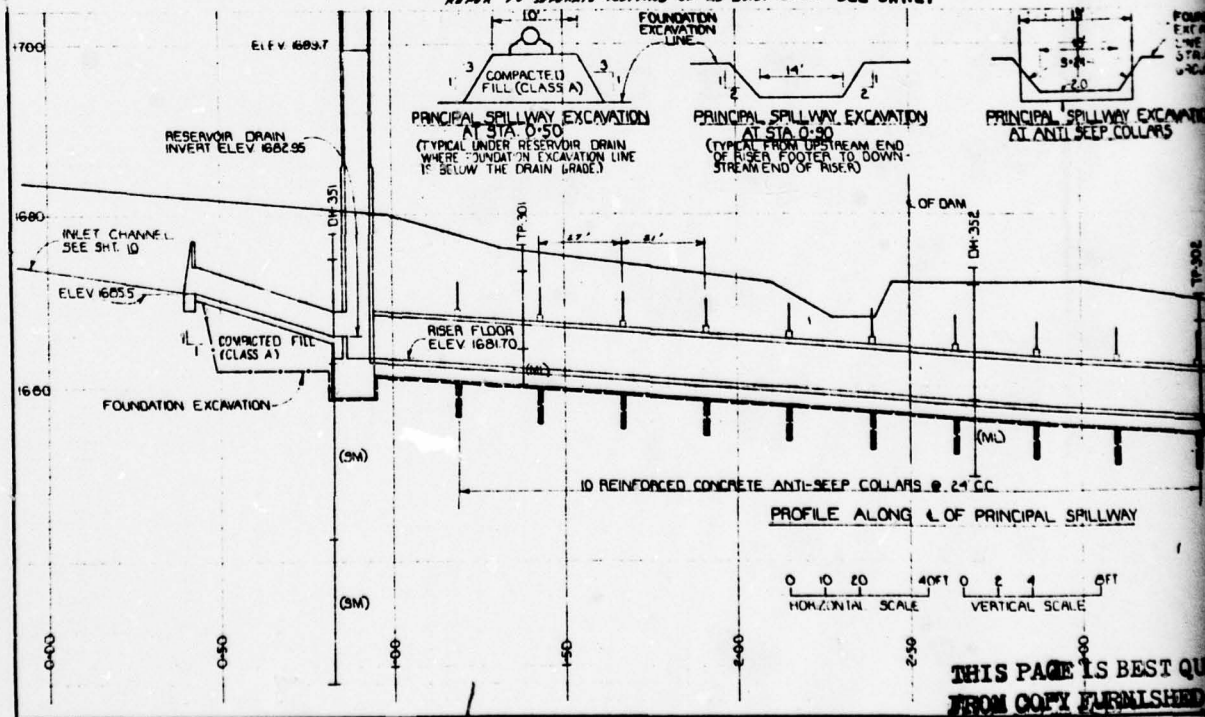
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SECTION OF DAM AT STATION 7+50

(TYPICAL FROM APPROX. STA. 1+20 TO APPROX. STA. 12+18)
REFER TO SEPARATE NOTTING OF AS BUILT ZONES SEE SHT. 27



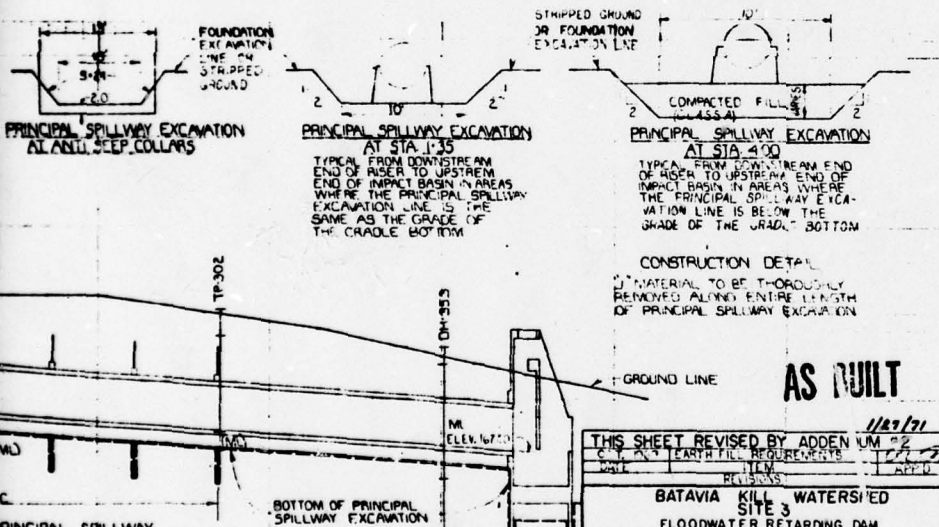
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EARTH FILL REQUIREMENTS						
ZONE	MATERIAL 1/	MAX. ROCK SIZE	MAX. LIFT THICK	MINIMUM REQUIRED MOISTURE CONTENT 2/	COMPACTION 3/	
					CLASS	DEFINITION
1	Materials A and B labelled on sheet 19 and represented by: TP 112 From 1.5' to 4.5' TP 113 From 1.5' to 11.5' TP 114 From 1.5' to 9.5' TP 115 From 1.5' to 9.5'	12"	4"	The water content of the material passing the 1/4" sieve shall be not less than 5 percent nor greater than 15 percent, unless notified by the field by the engineer near the line of construction.	2	See Construction Specification 5
2	represented by material in zone 1 plus materials C and D as labelled on sheet 20 and represented by: DM 241 From 1.5' to 14.5' DM 242 From 1.5' to 15.5' DM 243 From 1.5' to 25.5'	6"	4"	percent as noted below optimum	A	100% standard density by ASD method A
3	Material E as labelled on sheet 20 and represented by: TP 116 From 1.5' to 4.5' TP 117 From 1.5' to 7.5'	12"	1"	Met 5/		See Construction Specification 5

- 1/ The placement table indicates estimated use of material. Materials 1 and 2 as labelled on sheet 2 and represented by:
TP 112 From 1.5' to 12.5' and
TP 113 From 1.5' to 15.5'
will be utilized in the downstream section of zone 2 and 3.
- 2/a. Maximum rock size placed in backfill connected by means of hand rapping or manually directed power tampers or plate vibrators shall be 12".
- b. Oversize material greater than 6" in size from zone 2, that is, not used in the construction of the stone gutter will be utilized in zone 2 and 3.
- c. Oversize material greater than 6" is to be spread with zone 1 and 3, so that the larger rocks are placed toward the outside slopes. Oversize material will not be exposed on the outside slopes.
- 3/ Maximum lift thickness prior to compaction.
- 4/ Water content at time of compaction.
- 5/ Thoroughly wet but not so wet as to cause adherence of the soil to the wheels or tracks of equipment, nor to cause bogging down of equipment.
- 6/ For typical connection curves see sheet 22.

CONSTRUCTION DETAILS

1. The foundation surface throughout the base area of the dam shall be scarified to a depth of 6 inches and compacted prior to placement of material.
2. Zone boundaries indicated are approximate. Attention will be given by the engineer to permit the contractor to utilize all material required excavation within the wet lines of the abutments.
3. Material that is suitable for use and of sound quality in the specified area of the principal spillway shall be placed within the slope of the earth fill as directed by the engineer.



THIS SHEET REVISED BY ADDEN UM 11/25/71	
NO. 1	REVISIONS
BATAVIA KILL WATERSHED SITE 3 FLOODWATER RETARDING DAM GREENE COUNTY, NEW YORK FILL PLACEMENT & PRIN. SPWY EXCAV. U.S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE	
JE. POLLOCK	1169
R. E. VITA JR.	1169
J. DE VITA III	1169
22	NY-2153-D

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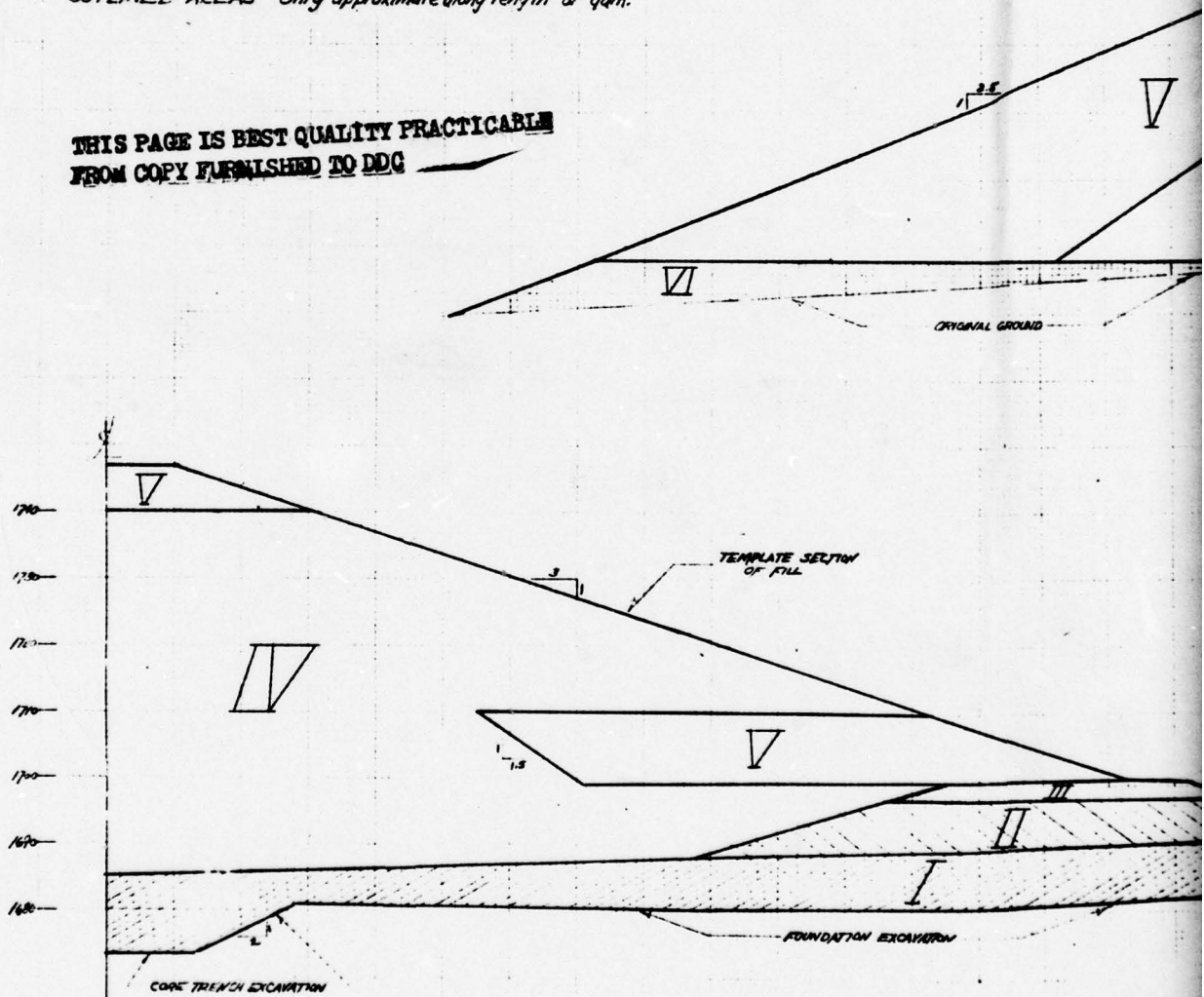
LEGEND

- AREA I - Placed under Zone 2 Specs; material A
- AREA II - Placed under Zone 1 Specs; material A with same D+E
- AREA III - Placed under Zone 2 Specs; material A with increasing D+E
- AREA IV - Placed under Zone 2 Specs; material B, D, +E.
- AREA V - Placed under Zone 1 Specs; material B
- AREA VI - Placed under Zone 3 Specs; material J

NOTE

OUTLINED AREAS Only approximate along length of dam.

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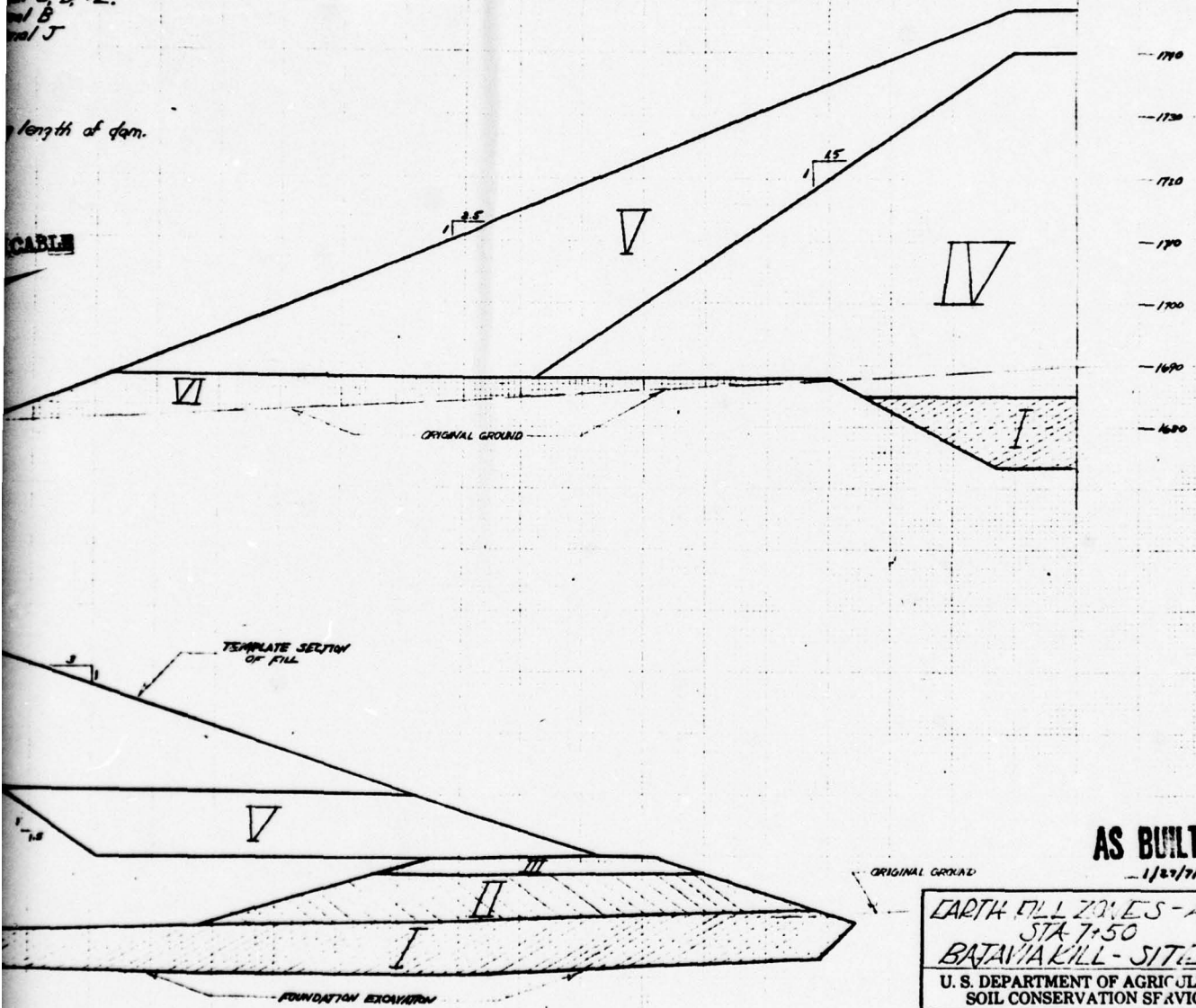


1 A
 1 A with same D+E
 1 A with increasing D+E
 1 B, D, +E.
 1 B
 1 J

length of dam.

CABLE

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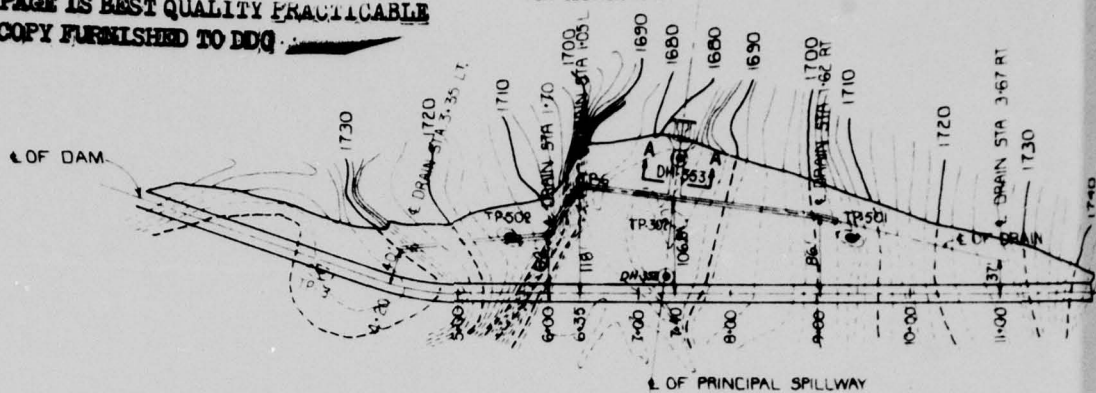
AS BUILT
 1/27/71

EARTH FILL ZONES - AT STA 7+50 BATAVIA KILL - SITE 3	
U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE	
Designed by _____ Drawn by _____ Traced by _____ Checked by _____	Date _____ Approved by _____ Title _____ Sheet No. 3 of 3 1/27/71

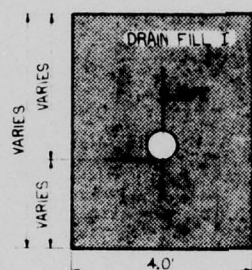
31-200-111 Rev. 6-69

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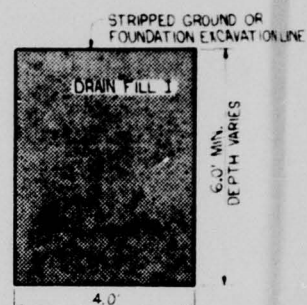
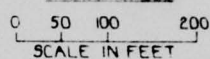
REFER TO SHEET 9
FOR SECTION A-A



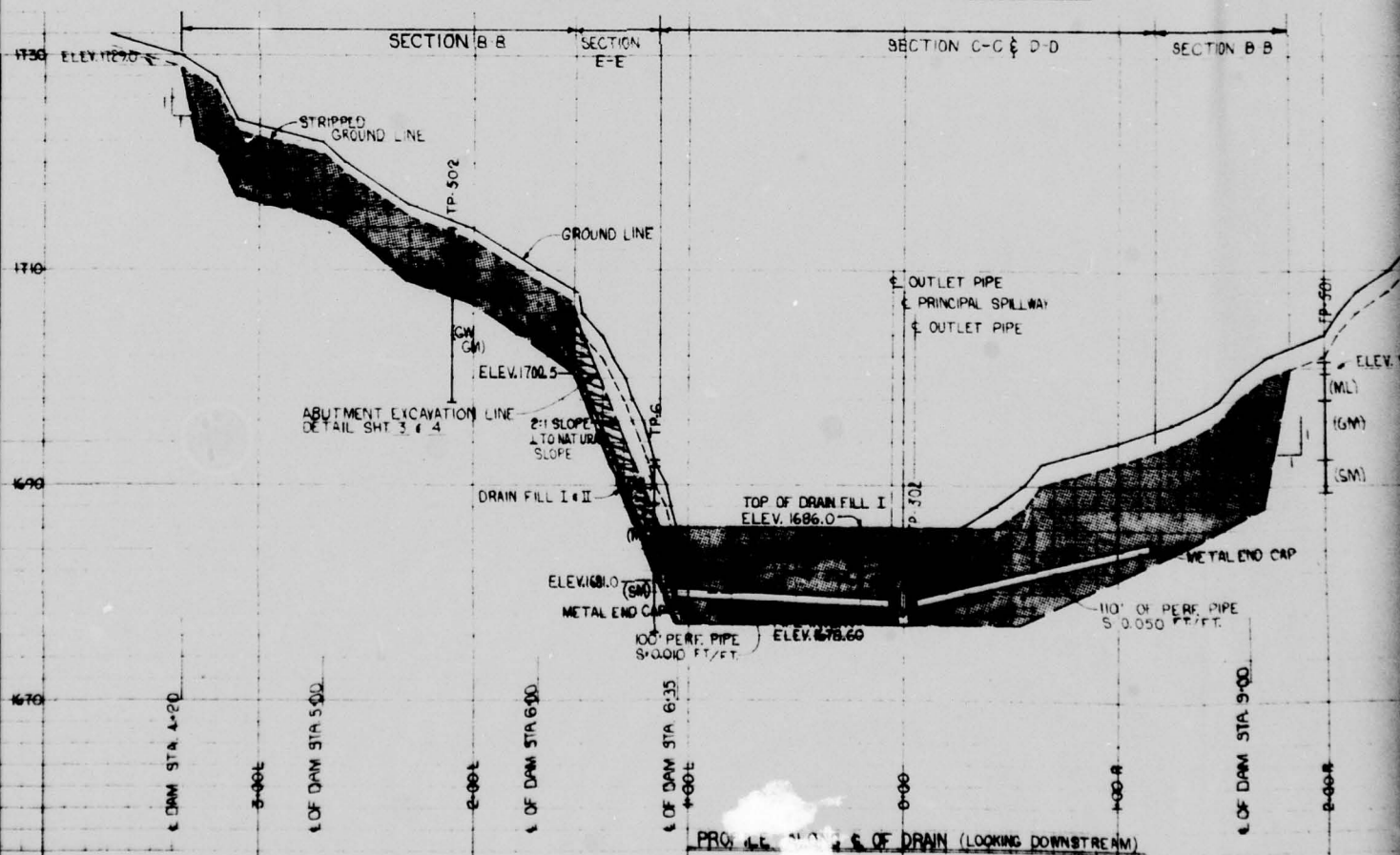
PLAN VIEW



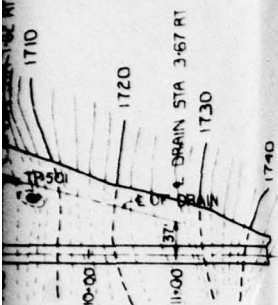
SECTION C-C & D-D



SECTION B-B



RAIN
ET 9



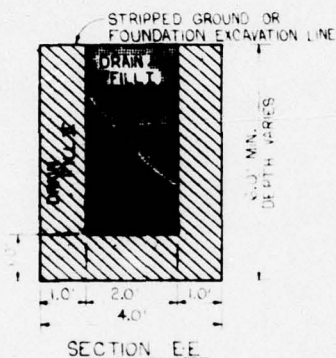
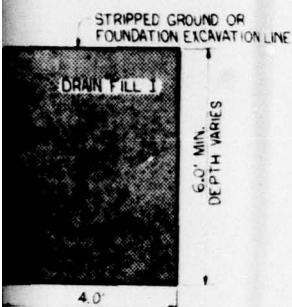
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DRAINAGE SYSTEM DETAILS

1. ALL DRAIN PIPE SHALL CONFORM TO SPEC. 110 AND SHALL BE 10" DIA., SHAPE I, CLASS I (ANNULAR CORRUGATIONS), OR CLASS II (HELICAL CORRUGATIONS), TYPE A (FULLY BITUMINOUS COATED) PIPE.
2. USE A MINIMUM OF 12" OF DRAIN FILL AROUND PIPE.
3. THE PROFILES AT THE BOTTOM OF ALL EXCAVATIONS AS SHOWN ARE ONLY APPROX. THE REQUIRED FINISHED GRADES WILL BE ESTABLISHED IN THE FIELD AT TIME OF CONSTRUCTION BY THE ENGINEER.

QUANTITY SUMMARY

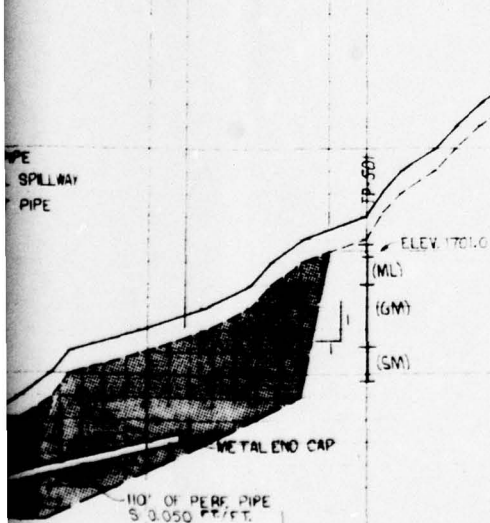
CU. YDS. DRAIN FILL I
CU. YDS. DRAIN FILL II
338 LIN. FT. 10" PERFORATED PIPE
2 METAL END CAPS
4 90° ELBOWS 10" DIA. (3 PIECE)
4 30° ELBOWS 10" DIA. (2 PIECE)



SECTION B-B

SECTION B-B

PIPE
SPILLWAY
PIPE



0 2 4 8 16
VERT. SCALE IN FEET

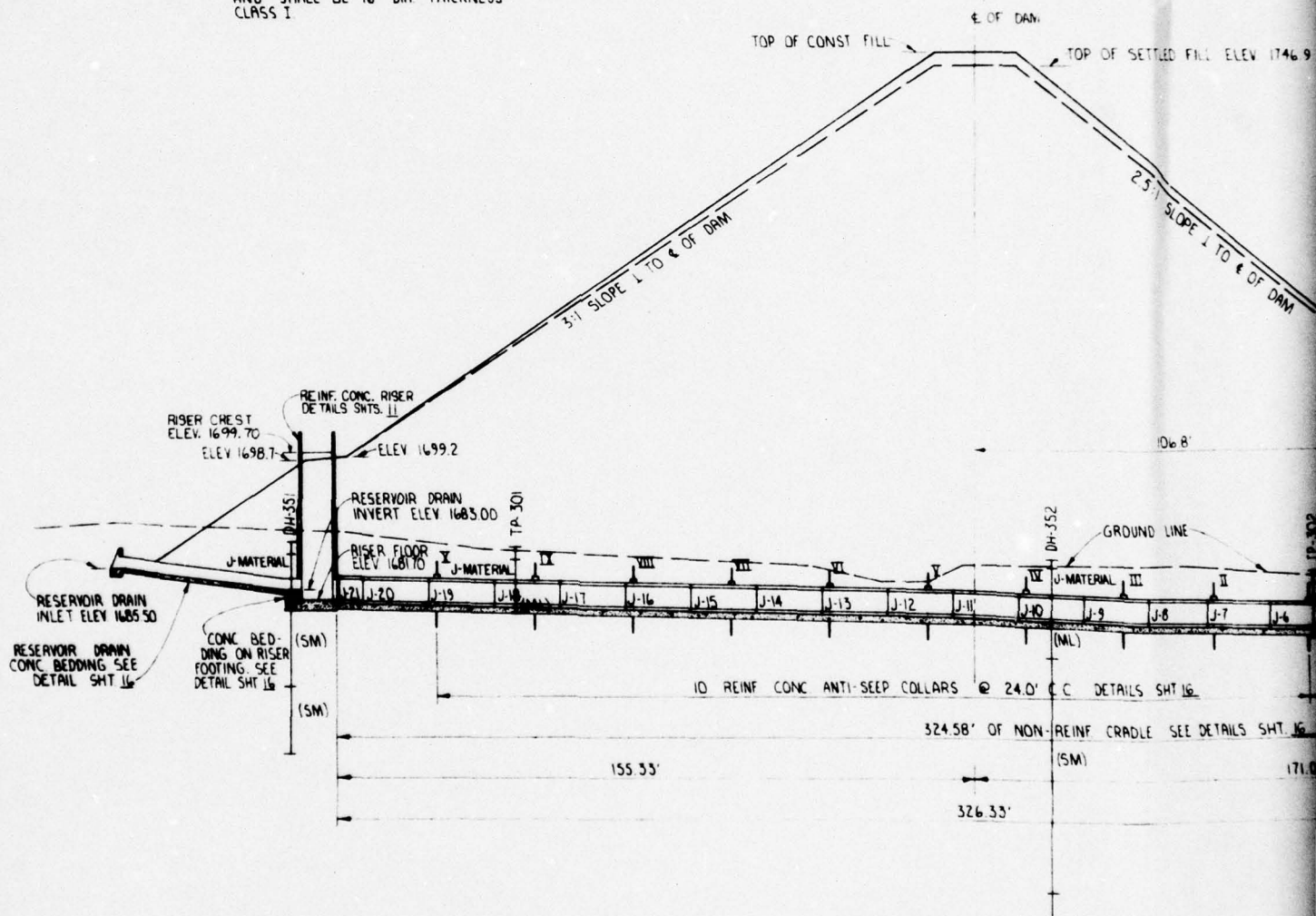
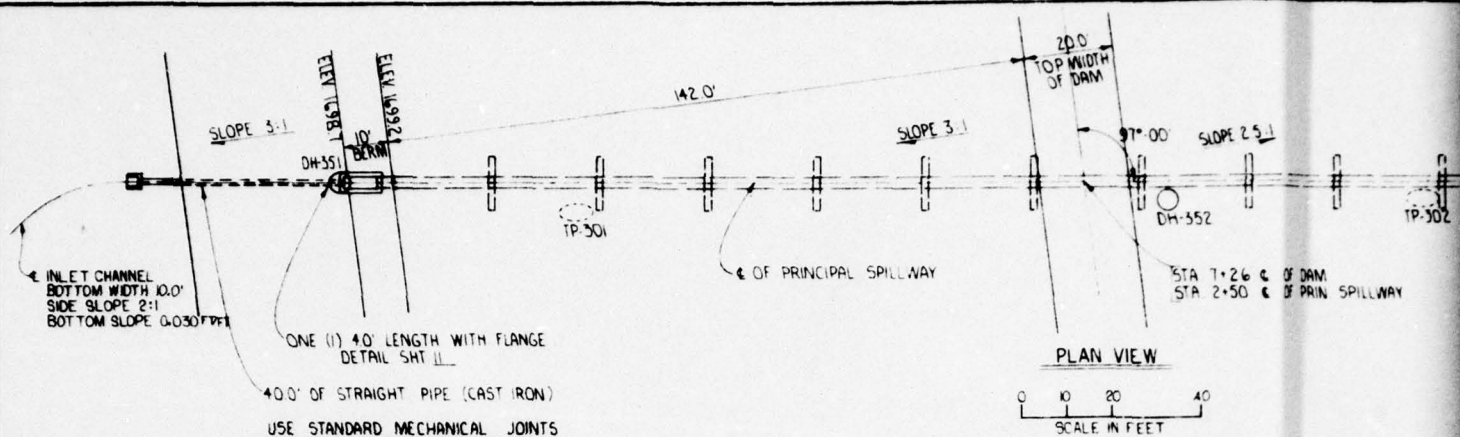
0 10 20 40 80
HORIZ. SCALE IN FEET

1+00
2+00
3+00
4+00
DAM STATION 1+00

BATAVIA KILL WATERSHED
SITE 3
FLOODWATER RETARDING DAM
GREENE COUNTY, NEW YORK
DRAINAGE SYSTEM DETAILS

U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

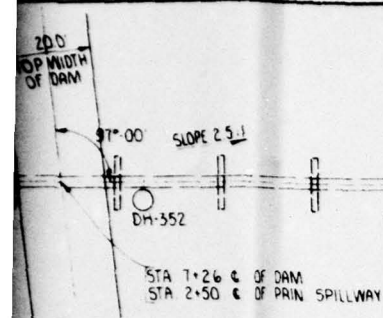
Designed J.E. POLULECH	Date 10/68	Approved by Title
Drawn D. ANGELO	Date 11/68	Title
Traced		
Checked J.E.P. DC CHAPMAN	Sheet 4/69 1/69	Drawing No. No. 8 22 NY-2153-P



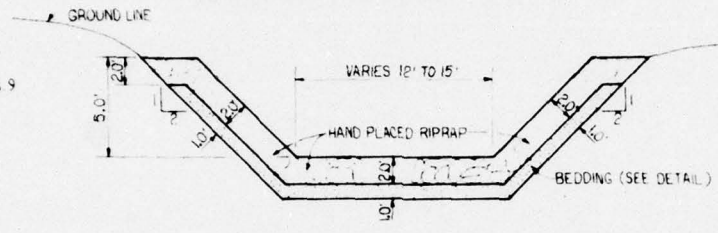
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0 10 20 40 FT
HORZ. SCALE

0 5 10 20 FT
VERT. SCALE



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SECTION A-A

RIPPRAP DETAILS

ALL RIPRAP SHALL BE GRADED FROM A MAX. SIZE OF 1 1/2" TO A MIN. SIZE OF 3/4". A LAYING OF RIPRAP SHALL BE LESS THAN 6" (≈ 1 LB.) AND A MAX. OF 12" SHALL BE LESS THAN 12" (≈ 40 LB.).
ADDITIONS ALL FILL THE GRADATION REQUIREMENTS FOR DRAIN FILL AS SHOWN ON SHEET 1.

JOINT	DIST FROM OUTLET	INVERT OF 30" DIA PIPE	SLOPE
OUTLET	0	1677.00	0.01127
J-1	16	1677.28	
J-2	32	1677.55	
J-3	48	1677.83	
J-4	64	1678.11	
J-5	80	1678.38	
J-6	96	1678.66	
J-7	112	1678.93	
J-8	128	1679.21	
J-9	144	1679.49	
J-10	160	1679.76	
J-11	176	1680.04	
J-12	192	1680.22	
J-13	208	1680.39	
J-14	224	1680.57	
J-15	240	1680.75	
J-16	256	1680.93	
J-17	272	1681.10	
J-18	288	1681.28	
J-19	304	1681.46	
J-20	320	1681.63	
J-21	326	1681.70	0.01107

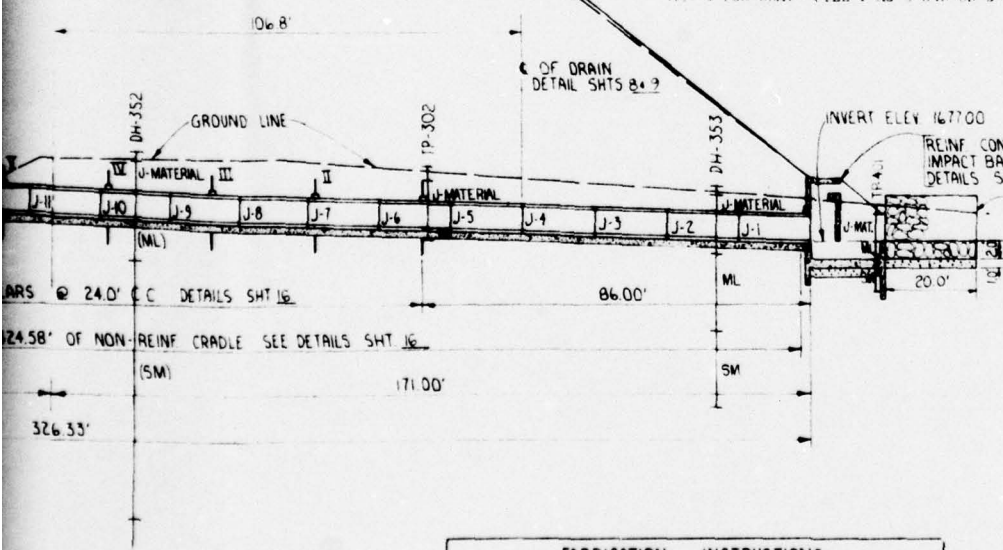
ABOVE DIMENSIONS FOR LENGTHS OF PIPE ARE BASED ON NOMINAL LENGTHS AND DO NOT INCLUDE CREEP

COLLAR	DIST FROM OUTLET	INVERT OF 30" DIA PIPE
I	86	1678.49
II	110	1678.90
III	134	1679.31
IV	158	1679.73
V	182	1680.11
VI	206	1680.37
VII	230	1680.64
VIII	254	1680.90
IX	278	1681.17
X	302	1681.43

30" REINFORCED CONCRETE PIPE STRENGTH REQUIREMENTS

1. PRESSURE HEAD 64 FT
2. LOAD 50,217 LBS PER LIN FT BASED ON O.D. OF 31.1 FT
3. MIN 3 EDGE BEARING STRENGTH FOR 0.001" CRACK 12,311 LBS PER LIN FT FOR PRESTRESSED PIPE (AWWA C-301)

WHERE THE PIPE FURNISHED HAS AN OUTSIDE DIAMETER GREATER THAN THAT CALLED FOR ON THE PLANS, THE THREE-EDGE BEARING STRENGTH OF THE PIPE FURNISHED MUST BE EQUAL TO OR GREATER THAN THE SPECIFIED THREE-EDGE BEARING STRENGTH MULTIPLIED BY THE RATIO OF THE OUTSIDE DIAMETER OF THE PIPE FURNISHED TO THE OUTSIDE DIAMETER SPECIFIED.



FABRICATION INSTRUCTIONS	
(20) 16'-0" SECTIONS (1) 6'-0" SECTION ONE (1) SPIGOT RING WALL FITTING FOR 18" WALL	(16) 20'-0" SECTIONS (1) 6'-0" SECTION ONE (1) SPIGOT RING WALL FITTING FOR 18" WALL
PIPE SUPPLIERS NOTE CAST OUTSIDE OF SPIGOT RING WITH CONCRETE ON ONE 16'-0" SECTION	OR PIPE SUPPLIERS NOTE CAST OUTSIDE OF SPIGOT RING WITH CONCRETE ON ONE 20'-0" SECTION

WHEN PIPE IS SUPPLIED IN 20'-0" LENGTHS THE ENGINEER WILL PROVIDE THE CONTRACTOR WITH A REVISION OF THIS SHEET SHOWING ORDER OF INSTALLATION AND PIPE INVERT ELEVATIONS

**BATAVIA KILL WATERSHED
SITE 3
FLOODWATER RETARDING DAM
GREENE COUNTY, NEW YORK
PLAN PROFILE OF PRINCIPAL SPILLWAY
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE**

Designed by: J.E. POLULECH 10/68
Checked by: W.E. GRAJDO JR. 10/68
Reviewed by: D.C. CHAPMAN 1/69

NY-2153-P

MATERIAL DESCRIPTIONS

A
Silt-sandy, trace to 5% gravel, 20-25% well graded sand, rest fines, brown, slightly moist, moderately permeable (k = 2.1 ft./day), medium to hard (N = 5-78, average 28 blows/ft.), derived from till through weathering and erosion. Sample 4.1 (ML)

B
Gravel-silty, trace to 10% +6" material (some boulders), 35-40% gravel, 30% sand, 30-40% slightly plastic fines, red-brown, moist, relatively impermeable, dense to very dense (N = 33-84, average 57 blows/ft.), glacial till. Samples: 501.1, 109.1, 207.1 (GM)

C
Gravel-sandy, trace of +6" material, 50-55% gravel, 35-40% sand, rest fines, occurs as interbedded sands and gravels w/occasional silt seams, brown, moist, moderately permeable (one test only, 2.4 ft./day), dense (N = 30-72 blows/ft.), outwash. (GM-GM) Samples: 3.1, 502.1

D
Silt-sandy, occasional +6" material, 5-10% gravel, 25-30% sand, 60-65% non-plastic silt, occurs as interbedded silts, sands, and gravels - description is a composite sample, brown, moist to saturated, moderately permeable (k = 0.0-21.4 averaging 3.0 ft./day), compact (N = 10-75, average 37 blows/ft.), glacial lacustrine. Sample 105.1 (ML)

E
Silt-clayey, occasional pieces of gravel, 10-15% fine and very fine sand; rest non-plastic fines, brown, moist, slightly permeable (k = 0.2-2.8 ft./day), firm (N = 17-39, average 30 blows/ft.), glacial lacustrine. Sample 206.1 (ML)

F
Sand-silty, trace of +6" material, 15% gravel, 60-65% well graded sand, 20-25% non-plastic fines; brown, moist, moderate permeability, compact (N = 27-118 average 53 blows/ft.), possible lacustrine. Sample 204.1 (SM)

G
Sand-silty, brown, moist, moderately plastic, relatively impermeable, hard (n = 53-190, average 113 blows/ft.), glacial till. (SM) Composite sample G

H
Sand-gravelly, 40-45% gravel, 45-50% sand, 15% fines, brown, moist, moderate to rapid permeability (k = 0.2-8.8 average 4.6 ft./day), very dense (N = 29-100, average 51 blows/ft.), valley fill deposit. Sample 501.2 (SM)

I
Sand-gravelly, 30-35% gravel, 55-60% sand, 10% non-plastic fines, brown, moist, moderate permeability, firm, outwash. (SW-SM) Sample 503.1

J
Recent alluvium - gravel - sandy, 5% +6" material, loose, rapid permeability, test holes cave badly and rapidly fill with water.

K
Topsoil, loose - organic matter, some stones and boulders - reddish-brown - permeable - average depth 1.0'.

BACKGROUND PIT LOGS

TP #1, C/L Elev. 1721.4

0	1.0	Material K
1.0	5.0	" A (ML)
5.0	11.0	" D (ML)
11.0	13.0	" H (SM)

TP #2, C/L Elev. 1694.9

0	1.0	Material K - v. stony
1.0	7.0	" B (GM)

TP #3, C/L Elev. 1732.2

0	1.0	Material K
1.0	3.0	" A (ML)
3.0	10.0	" C (GM-GM) D.S. 3.1
10.0	15.0	" I (SW-SM) D.S. 3.2

TP #4, C/L Elev. 1744.8

0	1.0	Material K
1.0	2.5	" A (ML) D.S. 4.1
2.5	11.0	" B (GM) D.S. 4.2

TP #5, C/L Elev. 1724.4

0	1.0	Material K
1.0	5.0	" I (SW-SM)
5.0	11.5	" C (GM-GM) D.S. 5.1

TP #6, C/L Elev. 1692.3

0	0.5	Rubble
0.5	4.0	Material E (ML)
4.0	9.0	" D (ML)
9.0	16.0	" H (SM)

TP #101, Borrow Area, Elev. 1724.9

0	1.0	Material K
1.0	4.0	" B (GM)
4.0	12.5	" D (ML) D.S. 101.1: 5.5'-5.7'
12.5+		Hole caving badly

W.L. 9.0' est. 9/29/67

TP #102, Borrow Area, Elev. 1713.4

0	1.0	Material K
1.0	5.5	" B (GM)
5.5	10.5	" D (ML)

W.L. 8.0' est. 9/29/67

TP #103, Borrow Area, Elev. 1733.8

0	1.0	Material K
1.0	3.0	" B (GM)
3.0	12.5	" D (ML)

TP #104, Borrow Area, Elev. 1754.7

0	1.0	Material K
1.0	9.0	" B (GM)

NOTE: Boulder & oversize count show 6-10%.

TP #105, Borrow Area, Elev. 1731.4

0	1.0	Material K
1.0	3.5	" A (ML)
3.5	6.0	" B (GM)
6.0	15.5	" D (ML) D.S. 105.1, @ 10.5'
15.5	16.0	" G (possibly) (SM)

TP #106, Borrow Area, Elev. 1728.5

0	1.0	Material K
1.0	5.0	" B (GM)
5.0	13.0	" D (ML)

TP #107, Borrow Area, Elev. 1744.1

0	1.0	Material K
1.0	8.0	" B (GM)
8.0	12.0	" D (ML) D.S. 107.1, 9.5'

NOTE: Sample of silt only.

TP #108, Borrow Area, Elev. 1738.7

0	1.0	Material K
1.0	6.0	" B (GM)
6.0	12.5	" D (ML)

TP #109, Borrow Area, Elev. 1750.3

0	1.0	Material K
1.0	10.0	" B (GM) D.S. 109.1, 10.0'

NOTE: Digging v. difficult.

TP #110, Borrow Area, Elev. 1726.1

0	1.0	Material K
1.0	4.5	" B (GM)
4.5	12.0	" D (ML)

TP #111, Borrow Area, Elev. 1740.5

0	1.5	Material K
1.5	12.0	" B (GM)

NOTE: Digging v. difficult.

TP #114, Borrow Area, Elev. 1801.7

0	1.0	Material K
1.0	9.0	" B (GM) D.S. 114.1

NOTE: Slightly stonier below 7.0'.

TP #115, Borrow Area, Elev. 1791.5

0	1.0	Material K
1.0	9.0	" B (GM) D.S. 115.1, 10.0'

NOTE: Slightly stonier below 7.0'.

TP #116, Borrow Area, Elev. 1808.2

0	1.0	Material K
1.0	13.0	" B (GM)

NOTE: Slightly stonier below 7.0'.

TP #117, Borrow Area, Elev. 1816.7

0	1.0	Material K
1.0	10.0	" B (GM)

NOTE: Slightly stonier below 7.0'.

TP #118, Borrow Area, Elev. 1797.3

0	1.0	Material K
1.0	10.0	" B (GM)

NOTE: Slightly stonier below 7.0'.

TP #201, Emer. Spillway, Elev. 1744.5

0	1.0	Material K
1.0	5.5	" A (ML)
5.5	14.0	" E (ML)
14.0	15.0	" F (SM)

TP #107, Borrow Area, Elev. 1744.3

0	1.0	Material K	
1.0	8.0	"	B (GM)
8.0	12.0	"	D (ML) D.S. 107.1, 9.5'

NOTE: Sample of silt only.

TP #108, Borrow Area, Elev. 1738.7

0	1.0	Material K	
1.0	6.0	"	B (GM)
6.0	12.5	"	D (ML)

TP #109, Borrow Area, Elev. 1750.3

0	1.0	Material K	
1.0	10.0	"	B (GM) D.S. 109.1, 10.0'

NOTE: Digging v. difficult.

TP #110, Borrow Area, Elev. 1726.1

0	1.0	Material K	
1.0	4.5	"	B (GM)
4.5	12.0	"	D (ML)

TP #111, Borrow Area, Elev. 1760.6

0	1.5	Material K	
1.5	12.0	"	B (GM)

NOTE: Digging v. difficult.

TP #114, Borrow Area, Elev. 1801.7

0	1.0	Material K	
1.0	9.0	"	B (GM) D.S. 114.1

NOTE: Slightly stonier below 7.0'.

TP #115, Borrow Area, Elev. 1791.5

0	1.0	Material K	
1.0	9.0	"	B (GM) D.S. 115.1, 10.0'

NOTE: Slightly stonier below 7.0'.

TP #116, Borrow Area, Elev. 1808.2

0	1.0	Material K	
1.0	13.0	"	B (GM)

NOTE: Slightly stonier below 7.0'.

TP #117, Borrow Area, Elev. 1816.7

0	1.0	Material K	
1.0	10.0	"	B (GM)

NOTE: Slightly stonier below 7.0'.

TP #118, Borrow Area, Elev. 1797.5

0	1.0	Material K	
1.0	10.0	"	B (GM)

NOTE: Slightly stonier below 7.0'.

TP #201, Emer. Spillway, Elev. 1744.5

0	1.0	Material K	
1.0	5.5	"	A (ML)
5.5	14.0	"	E (ML)
14.0	15.0	"	F (SM)

TP #202, Emer. Spillway, Elev. 1758.4

0	1.0	Material K	
1.0	8.0	"	A (ML)
8.0	15.0	"	I (SW-SM)

TP #203, Emer. Spillway, Elev. 1766.3

0	1.0	Material K	
1.0	6.0	"	A (ML)
6.0+			Refusal on boulders

TP #204, Emer. Spillway, Elev. 1759.1

0	1.0	Material K	
1.0	6.5	"	A (ML)
6.5	12.5	"	F (SM) D.S. 204.1

TP #205, Emer. Spillway, Elev. 1754.6

0	1.0	Material K	
1.0	16.0	"	E (ML)

TP #206, Emer. Spillway, Elev. 1751.1

0	1.0	Material K	
1.0	14.0	"	E (ML) D.S. 206.1

TP #207, Emer. Spillway, Elev. 1748.6

0	1.5	Material K	
1.5	10.0	"	B (GM) D.S. 207.1 @ 6.0'

TP #208, Emer. Spillway, Elev. 1740.2

0	1.5	Material K	
1.5	8.5	"	B (GM)

TP #209, Emer. Spillway, Elev. 1761.0

0	1.5	Material K	
1.5	9.0	"	B (GM)

TP #301, Prin. Spillway, Elev. 1688.2

0	1.5	Material K	
1.5	6.0	"	J
6.0	8.0	"	D (ML)

NOTE: Hole filling rapidly w/water and caving badly.

TP #302, Prin. Spillway, Elev. 1685.2

0	1.5	Material K	
1.5	7.0	"	J
7.0	8.0	"	D (ML)

NOTE: Hole filling rapidly w/water and caving badly.

TP #401, Stream Channel, Elev. 1681.0

0	1.0	Material K	
1.0	4.0	"	J
4.0	5.5	"	D (ML)
5.5	9.5	"	H (SM)

NOTE: Hole caving badly w/water entering rapidly.

WL est. @ 3.0' 9/28/67.

TP #501, Drain Line, Elev. 1771.5

0	1.0	Material K	
1.0	3.5	"	A (ML)
3.5	9.0	"	B (GM) D.S. 501.1 @ 8.0'
9.0	12.0	"	H (SM) D.S. 501.2 @ 9.5'

TP #502, Drain Line, Elev. 1711.9

0	1.0	Material K	
1.0	3.0	"	A (ML)
3.0	16.0	"	C (GM-GM) D.S. 502.1 @ 9.0'

TP #503, Drain Line, Elev. 1728.1

0	1.0	Material K	
1.0	4.0	"	A (ML)
4.0	7.0	"	I (SW-GM) D.S. 503.1 @ 5.0'
7.0	12.0	"	C (GM-GM) D.S. 503.2 @ 12.0'

DRILL HOLE LOGS

DM #51, C/L, Elev. 1728.5

0.0	Material K
1.0	
5	
6	Material A (ML)
8	
3.8	
16	
19	
19	Material D (ML)
15	
10	
66	
14.0	
29	
72	Material H (SM)
69	
20.0	
32	
91	
75	Material D (ML)
42	
38	
113	
28.0	
85	Material G (SM)
30.0	

WL Dry: 11/13/67

NOTE: Hole caved below 14.7'

DM #52, C/L, Elev. 1700.2

0.0	Material K
1.0	
33	
54	
84	Material B (GM)
58	
7.0	
35	
43	
49	
43	
37	
36	Material H (SM)
34	
38	
27	
37	
26.0	
31	
39	
30	Material D (ML)
27	
40	
38	
58	
37.0	
76	
53	Material C (SM)
92	
42.0	

WL 13.7' - 10/31/67; 12.8' - 11/13/67.

NOTE: Hole caved below 13.5'.

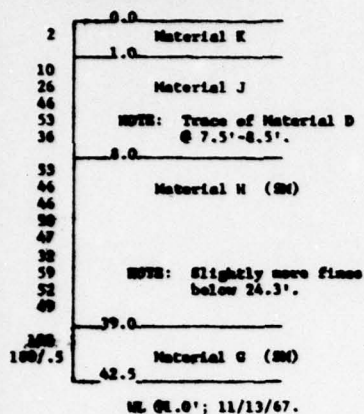
BATAVIA KILL WATERSHED
SITE 3
FLOODWATER RETARDING DAM
GREENE COUNTY, NEW YORK
LOGS OF TEST HOLES

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

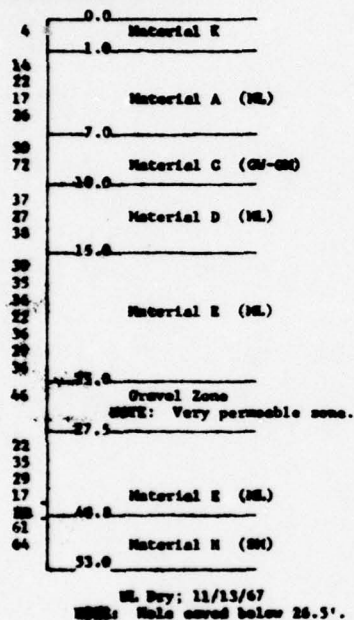
Project	Hamilton C. Page	Date	11/27
Drawn		By	H. J. Thomas
Checked		1 - STATE CONC. ENGR.	
Field No.		20	NY-2153-P
Scale		22	

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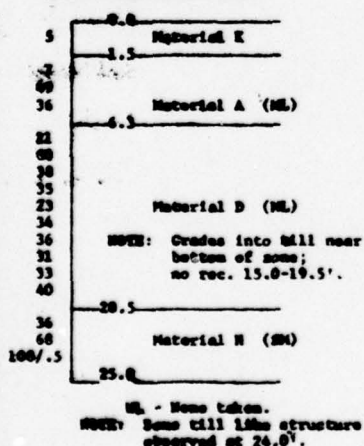
BN #23, C/L Elev. 1695.8



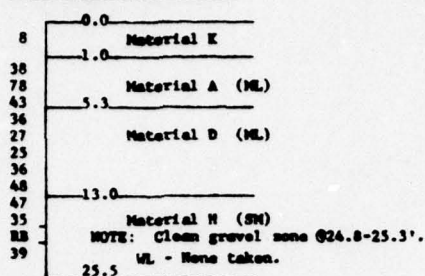
BN #24, C/L Elev. 1728.8



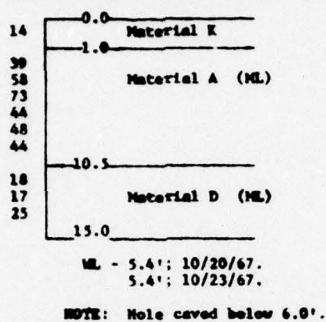
BN #25, C/L Elev. 1725.5



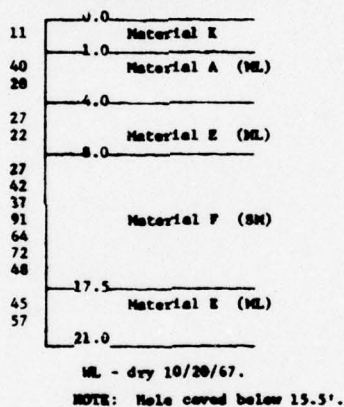
BN #26, C/L Elev. 1720.2



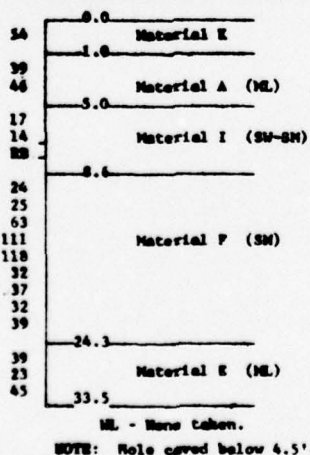
BN #251, Rmr. Spillway Elev. 1747.0



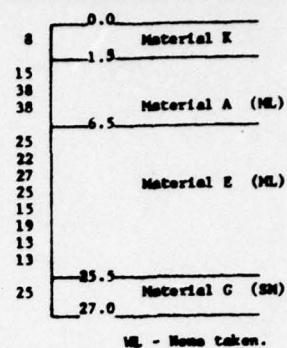
BN #252, Rmr. Spillway Elev. 1751.2



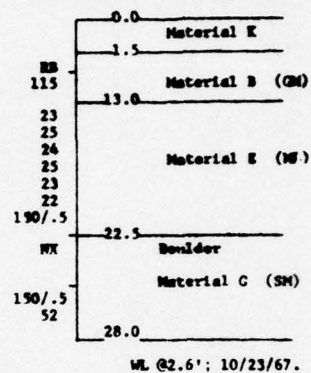
BN #253, Rmr. Spillway Elev. 1773.4



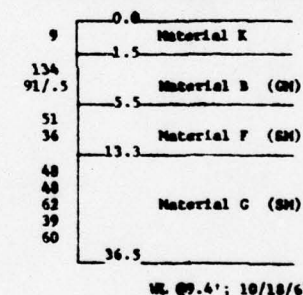
BN #254, Rmr. Spillway Elev. 1741.5



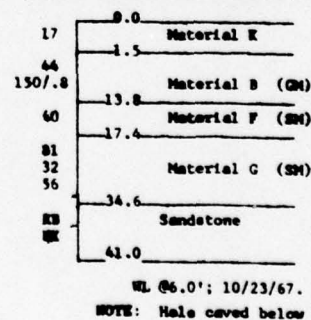
BN #255, Rmr. Spillway Elev. 1741.5



BN #256, Rmr. Spillway Elev. 1776.5



BN #257, Rmr. Spillway Elev. 1773.9



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254. River Spillway, Elev. 1741.5

0.0
Material K
1.5
Material A (NL)
6.5
Material E (NL)
35.5
Material G (SM)
27.0
NL - None taken.

251. Prin. Spillway, Elev. 1688.9

0.0
7
Material K
1.5
Material J
7.5
Material H (SM)
32
28
24
43
150/.7
63
NOTE: Some till like zones.
124/.5
1.7
100/.3
Material G (SM)
25.8
WL @ 2'; 11/13/67

253. River Spillway, Elev. 1741.5

0.0
Material K
1.5
Material B (SM)
13.0
Material E (NL)
22.5
Boulder
Material G (SM)
28.0
WL @ 2.6'; 10/23/67.
NOTE: Hole caved below 8.5'.

252. Prin. Spillway, Elev. 1688.9

0.0
5
Material K
1.0
Material J
7.6
Material D (NL)
12.0
Material H (SM)
28
36
37
73
44
44
58
38
33
37
32
34
142/.7
43
67
60
96
38
40.5
146/.5
BB Boulder
175/.6
150/.4
100/.2
Material G (SM)
56.0
Sandstone
61.0
WL - 2.7'; 11/6/67.
3.2'; 11/13/67.

256. River Spillway, Elev. 1776.5

0.0
Material K
1.5
Material B (SM)
5.5
Material F (SM)
13.3
Material G (SM)
36.5
WL @ 9.4'; 10/18/67.
NOTE: Hole caved below 9.5'.

253. Prin. Spillway, Elev. 1688.9

0.0
17
Material K
1.0
Material J
7.5
Material D (NL)
21
86/.6
BB Boulder
25
48
16.0
Material H (SM)
111
163/.7
59/.5
NOTE: Some till like zones present.
24.5
WL @ 1.3'; 11/6/67.
1.5'; 11/13/67.

257. River Spillway, Elev. 1773.9

0.0
Material K
1.5
Material B (SM)
13.8
Material F (SM)
17.4
Material G (SM)
34.6
Sandstone
43.0
WL @ 6.0'; 10/23/67.
NOTE: Hole caved below 11.3'.

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5

251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
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253. River Spillway, Elev. 1741.5
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257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
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253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

254. River Spillway, Elev. 1741.5
251. Prin. Spillway, Elev. 1688.9
253. River Spillway, Elev. 1741.5
252. Prin. Spillway, Elev. 1688.9
256. River Spillway, Elev. 1776.5
253. Prin. Spillway, Elev. 1688.9
257. River Spillway, Elev. 1773.9

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2

DM #254, Emergency Spillway, Elev. 1770.2

5	0.0	Material K
	1.0	
9	3.0	Material A (ML)
60/.3		
RB		Material B (GM)
46		Boulders 3.8-5.1
33		5.1-5.8
23		Poor rec. 9.0-10.5
	10.0	
18		Material E (ML)
33		
	13.3	
49		Material F (SM)
39		
	17.0	
18		Material E (ML)
12		v. soft 18.5-19.5
34		
	21.9	
34		
35		Material C (SM)
88		
Aug	41.0	

WL 4.9', 4/10/68. Hole caved below 8.7'

DM #259, Emergency Spillway, Elev. 1766.7

8	0.0	Material K
	1.0	
20/.1		Material A (SM)
	3.0	Boulder 2.1-3.0
RB		
RB		Material D (ML)
23		
	7.0	
RB		Material E (ML)
146		Boulder 8.9-12.0
28		Occasional 3" sand zones
46		
26		
	20.5	
33		Material F (SM)
30		Note apparent free water at 20.4'
63		
	24.6	
67		
RB		Material G (SM)
Aug		
	35.0	

WL Dry, 4/10/68.
Hole caved below 11.0'

DM #260, Emergency Spillway, Elev. 1772.4

8	0.0	Material K
	1.0	
37		
RB		Material A (ML)
117		Boulder 3.5-4.0
RB		Cobble 5.7-6.0
	6.0	
41		
46		Material D (ML)
34		
67		
	14.0	
83/.3		
RB		Material C (SM)
70		
RB		
34		Boulder 14.8-16.0, 17.6-18.5,
39		18.5-22 reworked till w/some
109		silt layers
136		
141		
71		
Aug		
	30.0	

WL 10.50's 4/10/68
Hole caved below 15.5'

DM #261, Emergency Spillway, Elev. 1781.1

20	0.0	Material K
	1.0	
15		Material A (ML)
	2.5	
20		
18		
19		Material F (SM)
13		
20		Mostly gravel - 28.0-30.0
32		Boulder 30.7-32.0
25		
47		
38		
51		
57		
46		
76		
120/.2		
RB		
64		35.0
29		
31		Material E (ML)
14		
41		41.0
37		
31		Material D (ML)
23		
	48.5	
34		Material G (SM)
34		Soft near top
133		55.0

WL dry, 4/10/68,
Hole caved below 34.0

DM #262, Emergency Spillway, Elev. 1770.1

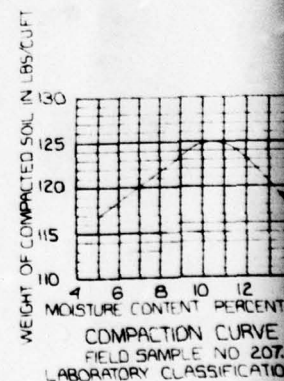
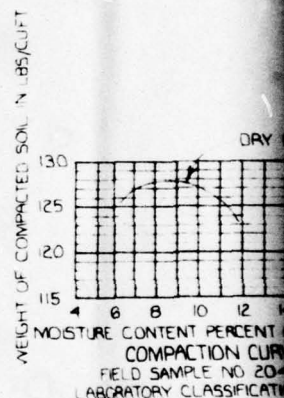
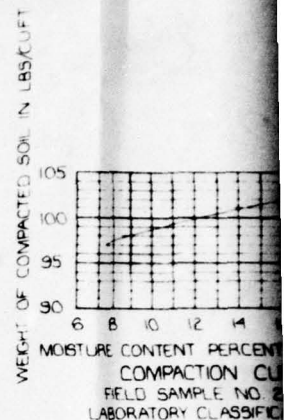
11	0.0	Material K
	1.0	
41		Material A (ML)
	4.5	
38		Material D (ML)
30		
39		8.8
25		
66		Material F (SM)
47		Numerous gradation variations
35		in samples
33		20.0
34		
20		
48		
35		
43		Material E (ML)
32		
RB		
49		
RB		
28		
RB		
	46.5	
19		Material G (SM)
Aug		47.0

WL dry, 4/10/68.
Hole caved below 5.5'

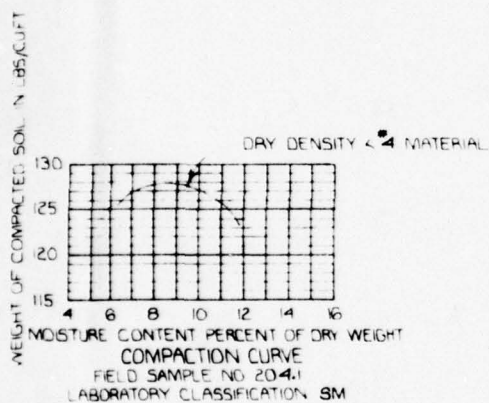
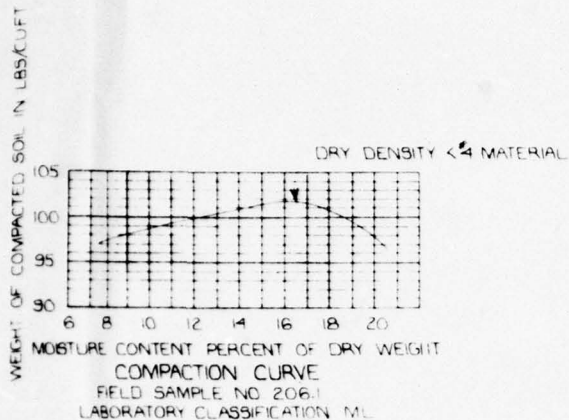
DM #263, Emergency Spillway, Elev. 1769.0

6	0.0	Material K
	1.0	
	1.5	Material A (ML)
74		
RB		Material F (SM)
28		Boulder 4.0-5.8
56		
	10.0	
8		
12		
29		Material E (ML)
11		Free water 19.0'
23		
22		
88		
29		26.0
37		
48		Material F (SM)
48		
	31.0	
34		
65		Material G (SM)
58		
76		
Aug		45.0

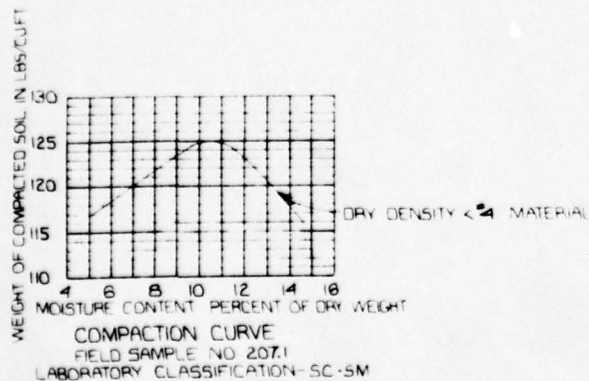
WL - none taken



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BATAVIA KILL WATERSHED
SITE 3
FLOODWATER RETARDING DAM
GREENE COUNTY, NEW YORK
LOGS OF TEST HOLES

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

DATE: 11/67
BY: RONALD C. PAGE

NY-2153-P

U.S. GPO: APRIL 1964

BATAVIA KILL SITE NO. 3 MM

EMBANKMENT AND FOUNDATION INPUT DATA

		FIRST POINT		SECOND POINT		DENSITY	SHEAR PARAMETERS		
		X	Y	X	Y	IN LBS/CU.FT.	ABOVE LINE PHI	C	BELOW PHI
LINE	1	-30.0	-7.2	-10.0	0.0	138.0	0.0	0.	36.0
LINE	2	-10.0	0.0	10.0	0.0	138.0	0.0	0.	36.0
LINE	3	10.0	0.0	155.0	-62.0	138.0	0.0	0.	36.0
LINE	4	-144.0	-48.2	-30.0	-7.2	-141.8	0.0	0.	36.0
LINE	5	-154.0	-48.2	-144.0	-48.2	-141.8	0.0	0.	36.0
LINE	6	-194.0	-62.0	-154.0	-48.2	-141.8	0.0	0.	36.0
LINE	7	-30.0	-7.2	107.0	-62.0	-141.8	36.0	300.	36.0
LINE	8	107.0	-62.0	155.0	-62.0	-141.8	36.0	300.	0.0
LINE	9	107.0	-62.0	-194.0	-62.0	-141.8	36.0	300.	0.0
LINE	10	-194.0	-62.0	-1000.0	-62.0	-141.8	0.0	0.	0.0
LINE	11	155.0	-62.0	1000.0	-62.0	-141.8	0.0	0.	0.0

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11X/14

Pg 5-1

ANKMENT AND FOUNDATION INPUT DATA

SECOND POINT		DENSITY IN LBS/CU.FT.	SHEAR PARAMETERS			
X	Y		ABOVE LINE		BELOW LINE	
			PHI	C	PHI	C
-10.0	0.0	138.0	0.0	0.	36.0	300. ✓
10.0	0.0	138.0	0.0	0.	36.0	300. ✓
155.0	-62.0	138.0	0.0	0.	36.0	300. ✓
-30.0	-7.2	-141.8	0.0	0.	36.0	300. ✓
-144.0	-48.2	-141.8	0.0	0.	36.0	300. ✓
-154.0	-48.2	-141.8	0.0	0.	36.0	300. ✓
107.0	-62.0	-141.8	36.0	300.	36.0	300. ✓
155.0	-62.0	-141.8	36.0	300.	0.0	0.
-194.0	-62.0	-141.8	36.0	300.	0.0	0.
1000.0	-62.0	-141.8	0.0	0.	0.0	0.
1000.0	-62.0	-141.8	0.0	0.	0.0	0.

VALUES FROM SOIL TEST RESULTS
3/69 FOR ZONE 1 MATERIAL
 $\phi = 36^\circ$ $C = 300$ P.S.F.
JEP 4-69

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Pg 5-1

A

BATAVIA KILL SITE NO. 3 MM

UPSTREAM SLOPE 100 PER CENT STANDARD DENSITY ON 4

ARC INPUT DATA

HORIZONTAL DISTANCE FROM CENTERLINE OF DAM TO LEFT MOST ARC CENTER = -160.0

HORIZONTAL DISTANCE BETWEEN ARC CENTERS = 10.0 FT.

NUMBER OF HORIZONTAL DISTANCES = 8

VERTICAL DISTANCE FROM TOP OF DAM TO UPPER MOST ARC CENTER = 168.0 FT.

VERTICAL DISTANCE BETWEEN ARC CENTERS = -10.0 FT.

NUMBER OF VERTICAL DISTANCES = 6

DISTANCE BETWEEN ARC RADIUS = 4 FT.

LINE NUMBER TANGENT TO MINIMUM ARC = 6

LINE NUMBER TANGENT TO MAXIMUM ARC = 9

MINIMUM SAFETY FACTOR AND ASSOCIATED RADIUS FOR SELECTED ARC CENTERS

VERTICAL DISTANCE	-160.0		-150.0		-140.0		-130.0		-120.0		-110.0		RA
	RAD	FS	RAD	FS	RAD	FS	RAD	FS	RAD	FS	RAD	FS	
168.0	230	1.799	230	1.795	230	1.834	222	1.899	218	1.964	214	2.083	21
158.0	220	1.802	220	1.783	220	1.807	212	1.871	208	1.925	208	2.029	20
148.0	210	1.813	210	1.774	210	1.786	206	1.840	198	1.891	198	1.980	19
138.0	200	1.828	200	1.773	200	1.770	196	1.815	188	1.859	188	1.934	18
128.0	190	1.849	190	1.781	190	1.759	190	1.792	178	1.829	178	1.894	17
118.0 PAUSE	180	1.876	180	1.793	180	1.754	180	1.771	168	1.806	168	1.861	16

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Pg 5-2

STANDARD DENSITY ON 4

ARC INPUT DATA

FROM CENTERLINE OF DAM TO LEFT MOST ARC CENTER = -160.0 FT.

BETWEEN ARC CENTERS = 10.0 FT.

DISTANCES = 8

TOP OF DAM TO UPPER MOST ARC CENTER = 168.0 FT.

BETWEEN ARC CENTERS = -10.0 FT.

DISTANCES = 6

RADIUS = 4 FT.

MINIMUM ARC = 4

MAXIMUM ARC = 9

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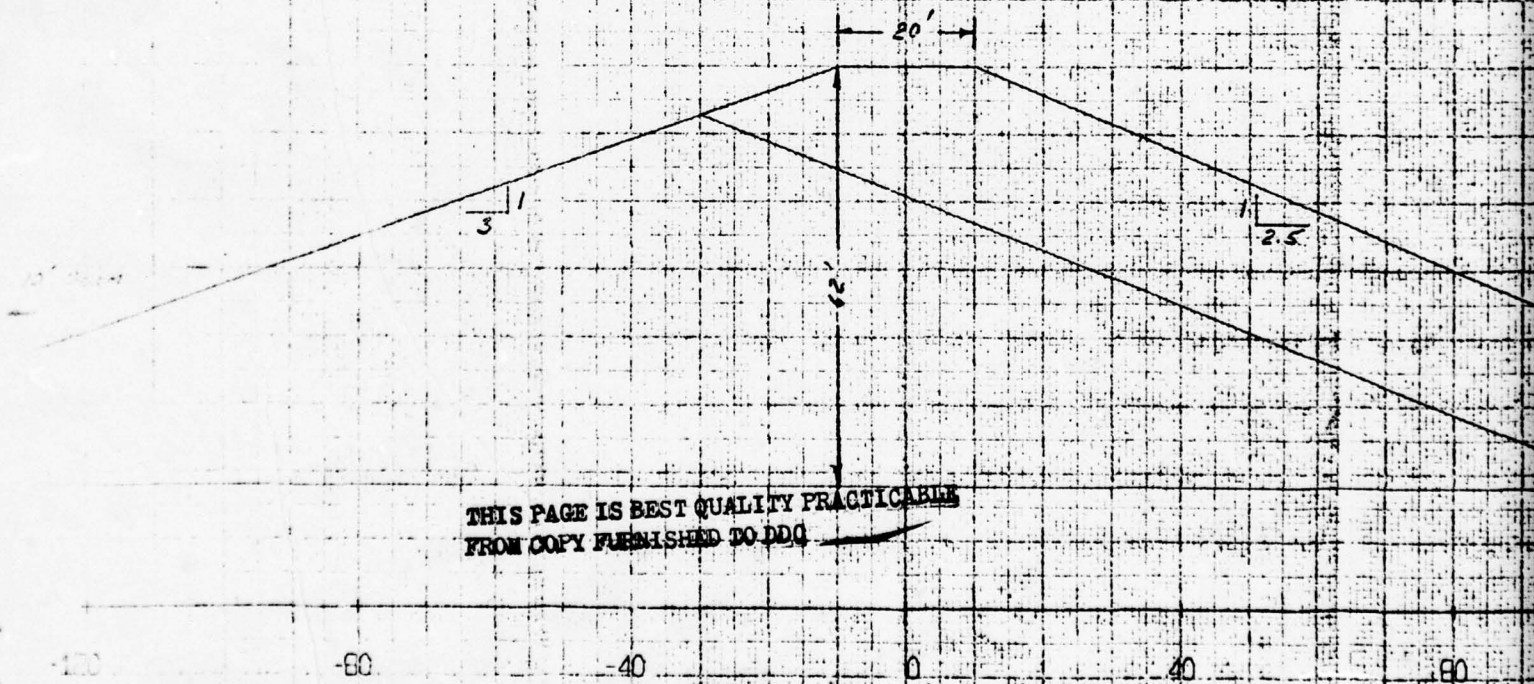
AND ASSOCIATED RADIUS FOR SELECTED ARC CENTERS

		HORIZONTAL DISTANCE									
		-130.0		-120.0		-110.0		-100.0		-90.0	
		RAD	FS	RAD	FS	RAD	FS	RAD	FS	RAD	FS
6	222	1.899		218	1.964	214	2.083	210	2.253	210	2.473
7	212	1.871		208	1.925	208	2.029	204	2.191	200	2.396
8	206	1.840		198	1.891	198	1.980	194	2.129	190	2.322
9	196	1.815		188	1.859	188	1.934	184	2.067	180	2.251
10	190	1.792		178	1.828	178	1.894	174	2.013	170	2.179
11	180	1.771		168	1.806	168	1.861	168	1.962	160	2.114

Pg 5-2

2

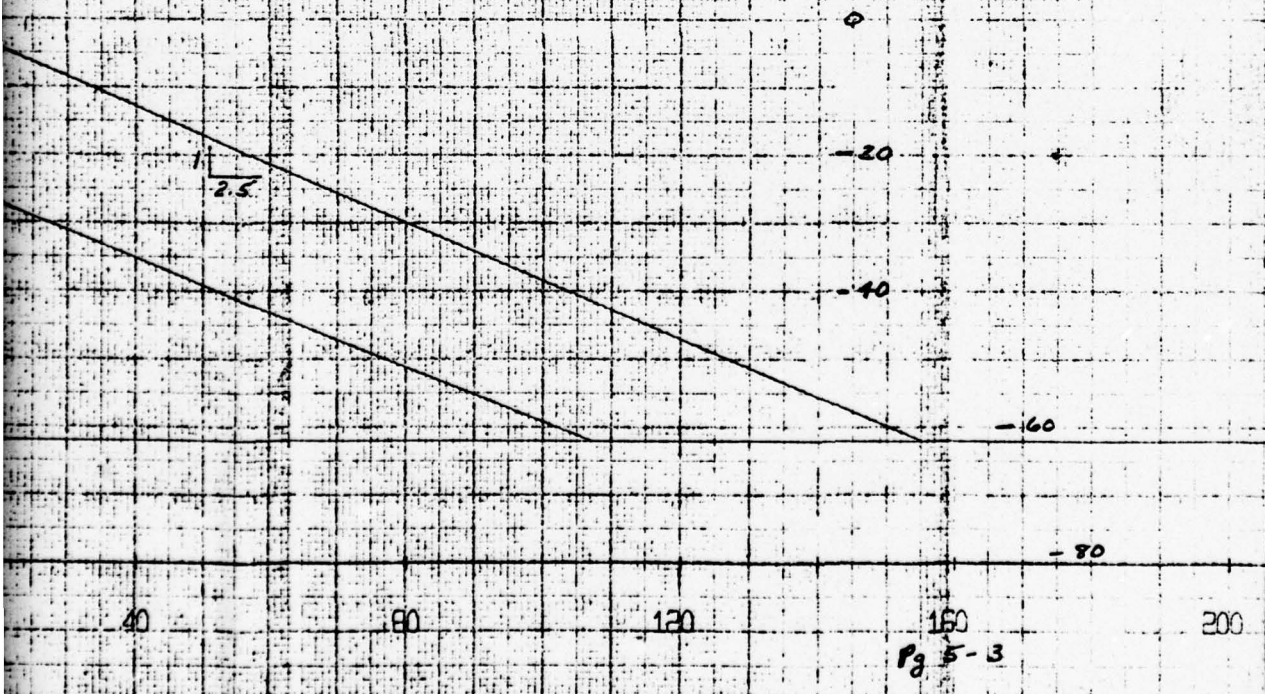
BATAVIA KILL SITE NO. 3 MM



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Pg 5-3

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APPENDIX B

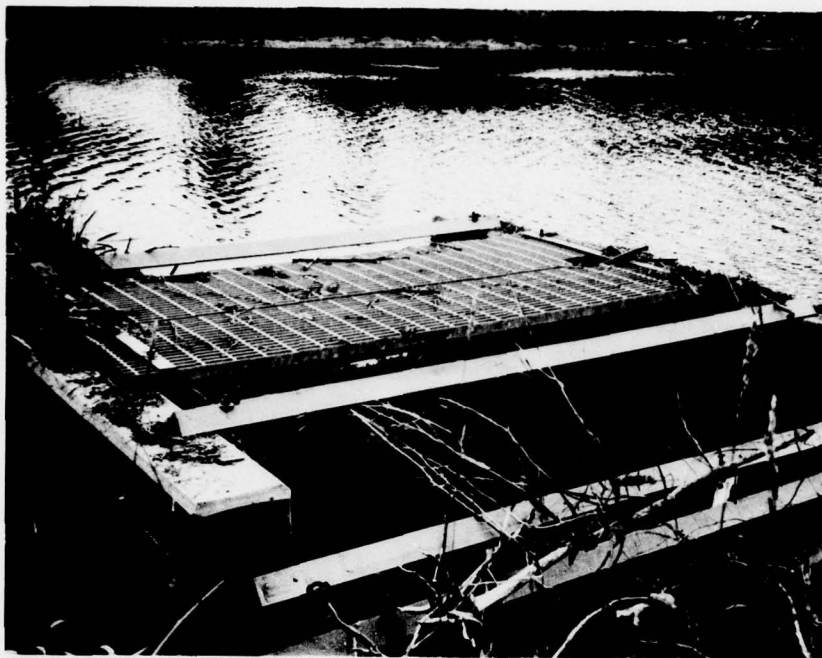
PHOTOGRAPHS



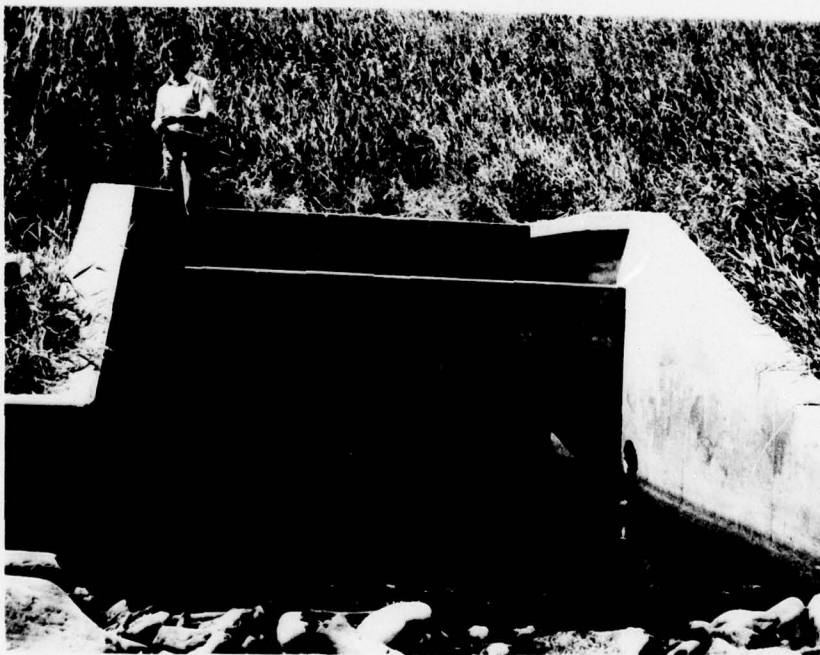
RESERVOIR POOL @ PRINCIPAL SPILLWAY
(looking East)



WEST EMERGENCY SPILLWAY



INLET of PRINCIPAL SPILLWAY
@ RISER



OUTLET of PRINCIPAL SPILLWAY
@ IMPACT BASIN

APPENDIX C

ENGINEERING DATA CHECKLIST

BAY...A
 Name of Dam DAM #3
 I.D. # NY-608
 (#191C-3818)

Check List
 Engineering Data
 Design Construction Operation

Item	Remarks
Plans	Details
YES	YES
Typical Sections	YES
Dam	YES
Spillway(s)	YES
Outlet(s)	YES
Design Reports	YES
Design Computations	
Discharge Rating Curves	
Dam Stability	
Seepage Studies	
Subsurface and Materials Investigations	YES

Item

Remarks

Construction History

Surveys, Modifications,
Post-Construction Engineering
Studies and Reports

NONE REPORTED

Accidents or Failure of Dam
Description, Reports

NONE REPORTED

Operation and Maintenance Records
Operation Manual

N/A

APPENDIX D

VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST

1) Basic Data

a. General

Name of Dam BATAVIA KILL WATERSHED PROJECT DAM No. 3

I.D. # NY-608 (#191C-3818)

Location: Town WINDHAM County GREENE

Stream Name UNNAMED TRIBUTARY TO BATAVIA KILL

Tributary of SCHOHARIE CREEK; MOHAWK RIVER BASIN

Longitude (W), Latitude (N) W 74°-13'-58" N 42°-19'-06"

Hazard Category C

Date(s) of Inspection JULY 11, 1978

Weather Conditions CLEAR 70°

b. Inspection Personnel KOCH MCCARTY BERQUIST
ISLAM HARMER

c. Persons Contacted H. HERTH (SCS) E. BLACKMER (SCS)

d. History:

Date Constructed 1970

Owner BATAVIA KILL WATERSHED DISTRICT

Designer SOIL CONSERVATION SERVICE (SCS)

Constructed by HALMAR CONSTR. CORP.

2) Technical Data

Type of Dam EARTH EMBANKMENT

Drainage Area 2304 ACRES

Height 63' Length 1100'

Upstream Slope 1:3 Downstream Slope 1:2.5

2) Technical Data (Cont'd.)

External Drains: on Downstream Face N/A @ Downstream Toe YES

Internal Components:

Impervious Core N/A

Drains UNDER DOWNSTREAM SLOPE

Cutoff Type EARTH TRENCH ; KEYED TO FOUNDATION SOILS

Grout Curtain N/A

3) Embankment

a. Crest

(1) Vertical Alignment GOOD

(2) Horizontal Alignment GOOD

(3) Surface Cracks NONE VISIBLE

(4) Miscellaneous

b. Slopes

(1) Undesirable Growth or Debris, Animal Burrows NONE

(2) Sloughing, Subsidence or Depressions NONE

(3) Slope Protection NO RIPRAP ON UPSTREAM FACE OF THE
EMBANKMENT AT ELEVATION OF PRINCIPAL SALLYWAY CREST

(4) Surface Cracks or Movement at Toe NONE

(5) Seepage NONE

(6) Condition Around Outlet Structure SATISFACTORY

c. Abutments

(1) Erosion at Embankment and Abutment Contact NONE

(2) Seepage along Contact of Embankment and Abutment NONE

(3) Seepage at toe or along downstream face NONE

d. Downstream Area - below embankment

(1) Subsidence, Depressions, etc. NONE

(2) Seepage, unusual growth NONE

(3) Evidence of surface movement beyond embankment toe NONE

(4) Miscellaneous

e. Drainage System

INTERNAL UNDER DOWNSTREAM FACE OF THE EMBANKMENT

(1) Condition of relief wells, drains, etc. N/A

(2) Discharge from Drainage System < 5 GPM ; FREELY FLOWING ; CLEAR ;
OUTLETED @ SIDEWALLS OF THE IMPACT BASIN

4) Instrumentation

(1) Monumentation/Surveys N/A

(2) Observation Wells N/A

(3) Weirs N/A

(4) Piezometers N/A

(5) Other

5) Reservoir

a. Slopes SATISFACTORY

b. Sedimentation N/A

6) Spillway(s): (including tail race channel)

WATER SURFACE ELEVATION SLIGHTLY ABOVE THE PRINCIPAL
SPILLWAY CREST

a. General

b. Principle Spillway 18' HIGH RECTANGULAR RC DROP INLET; 30" DIA.
RC PRESSURE PIPE; IMPACT BASIN

SATISFACTORY

c. Emergency or Auxiliary Spillway 2 GRASS-LINED TRAPEZOIDAL
OPEN CHANNELS IN EARTH CUTS; ONE EACH SIDE OF THE
MAIN EMBANKMENT SATISFACTORY EXCEPT THE
GRASS INVERTS NEED MOWING

d. Condition of Tail race channel SATISFACTORY

e. Stability of Channel side/slopes GOOD

7) Downstream Channel

a. Condition (debris, etc.) GOOD WITH SOME DEBRIS AND
LOGS SCATTERED ALONG THE INVERT

b. Slopes ERODED

c. Approximate number of homes 60 INCL. VILLAGE OF WINDHAM

8) Miscellaneous

9) Structural

a. Concrete Surfaces SATISFACTORY

b. Structural Cracking NONE

c. Movement - Horizontal & Vertical Alignment (Settlement) N/A

d. Junctions with Abutments or Embankments

e. Drains - Foundation, Joint, Face

f. Water passages, conduits, sluices

g. Seepage or Leakage N/A

h. Joints - Construction, etc. _____

i. Foundation _____

j. Abutments _____

k. Control Gates RESERVOIR DRAIN SLIDE GATE IS OPERATIONAL BUT
WAS NOT REPOSITIONED AT THE TIME OF INSPECTION

l. Approach & Outlet Channels _____

m. Energy Dissipators (~~plunge pool~~, etc.) IMPACT BASIN - SATISFACTORY

n. Intake Structures _____

o. Stability _____

p. Miscellaneous _____

APPENDIX E

HYDROLOGIC/HYDRAULIC ENGINEERING

DATA AND COMPUTATIONS

CHECK LIST FOR DAMS
HYDROLOGIC AND HYDRAULIC
ENGINEERING DATA

1

AREA-CAPACITY DATA:

	<u>Elevation</u> (ft.)	<u>Surface Area</u> (acres)	<u>Storage Capacity</u> (acre-ft.)
1) Top of Dam	<u>1746.9</u>	<u>71.0</u>	<u>1415</u>
2) Design High Water (Max. Design Pool)	<u>1741.9</u>	<u>59.0</u>	<u>1095</u>
3) Auxiliary Spillway Crest	<u>1739.7</u>	<u>54.3</u>	<u>975</u>
4) Pool Level with Flashboards	<u>N/A</u>	<u> </u>	<u> </u>
5) Service Spillway Crest	<u>1699.7</u>	<u>4.6</u>	<u>23.0</u>

DISCHARGES

	<u>Volume</u> (cfs)
1) Average Daily	<u>N/A</u>
2) Spillway @ Maximum High Water	<u>132</u>
3) Spillway @ Design High Water	<u>N/A</u>
4) Spillway @ Auxiliary Spillway Crest Elevation	<u>125</u>
5) Low Level Outlet	<u>28</u>
6) Total (of all facilities) @ Maximum High Water	<u>17600</u>
7) Maximum Known Flood	<u>90</u>

CREST:

ELEVATION: 1746.9Type: LEVEL - GRASSED EARTHWidth: 20' Length: 1100'Spillover N/A

Location _____

SPILLWAY:

PRINCIPAL

EMERGENCY

1699.7

Elevation

1739.7RC DROP INLET w/ TRASH RACK

Type

TRAPEZOIDAL OPEN CHANNELS2'-6" x 7'-6"

Width

EAST - 50' SLOPES: 1:3
WEST - 200'Type of Control✓

Uncontrolled

✓

Controlled:

N/A

Type

N/A

(Flashboards; gate)

N/A

Number

N/AN/A

Size/Length

N/A

Invert Material

MOWED GRASSAnticipated Length
of operating service< 1 PER 100 YRS30" DIA RC CONDUIT - 326' ~~Gate~~ Length EAST - 205' WEST - 690'SHARP-CRESTEDHeight Between Spillway Crest
& Approach Channel Invert
(Weir Flow)N/ABROAD-CRESTEDL/b = 1.0WEIR LENGTH = 15.0'

~~OUTLET STRUCTURES~~/EMERGENCY DRAWDOWN FACILITIES:Type: Gate ☒ Sluice _____ Conduit ☒ Penstock _____Shape : GATE - FLAT CIRCULAR CONDUIT - ROUND CAST IRONSize: GATE - 16" DIA. CONDUIT - 16" DIA.Elevations: Entrance Invert 1685.5Exit Invert 1682.95Tailrace Channel: Elevation 1677.0

HYDROMETEROLOGICAL GAGES:

Type : _____

Location: _____

Records:

Date - _____

Max. Reading - _____

FLOOD WATER CONTROL SYSTEM:

Warning System: NONE

Method of Controlled Releases (mechanisms):

N/A EXCEPT FOR RESERVOIR DRAIN SLIDE GATE - MANUALLY
OPERATED

DRAINAGE AREA: 2304 ACRES 3.6 SQ. MI.

DRAINAGE BASIN RUNOFF CHARACTERISTICS:

Land Use - Type: FARM FIELDS & WOODLANDS

Terrain - Relief: MODERATE TO STEEP w/ STEEPER SLOPES IN UPPER REACHES
OF WATERSHED

Surface - Soil: _____

Runoff Potential (existing or planned extensive alterations to existing
(surface or subsurface conditions)

NONE

Potential Sedimentation problem areas (natural or man-made; present or future)

N/A

Potential Backwater problem areas for levels at maximum storage capacity
including surcharge storage:

N/A

Dikes - Floodwalls (overflow & non-overflow) - Low reaches along the
Reservoir perimeter:

Location: NONE

Elevation: _____

Reservoir:

Length @ Maximum Pool N/A (Miles)

Length of Shoreline (@ Spillway Crest) N/A (Miles)

RUNOFF

(10.21)

BATAVIA KILL #3

①

$$\left. \begin{array}{l} P = 23 \\ CN = 80 \end{array} \right\}$$

$$Q = 20.3 (\text{in.})$$

$$CN(SCS) = 79 (\text{USE } 80)$$

#191C-3818

5 Hydrograph Family (21.83)

$$\left. \begin{array}{l} P = 23 \\ CN = 80 \end{array} \right\}$$

Hydrograph Family #1

$$\left[\begin{array}{l} \text{PMF} - 6 \text{ HOUR} \\ \leq 10 \text{ SQ MILES} \end{array} \right]$$

DRAINAGE AREA

2304 ACRES

or

3.6 SQ. MI.

6 Duration of Excess Rainfall (21.85)

$$\left. \begin{array}{l} P = 23 \\ CN = 80 \end{array} \right\}$$

$$T_o = 5.7 \text{ Hrs.}$$

7 $T_o = 1.32 \text{ Hrs.}$ (TIME OF CONCENTRATION)

$$T_p = .7 T_o$$

$$T_p = .7 (1.32) = 0.924 \text{ Hrs.}$$

$$\frac{T_o}{T_p} = 6.17$$

8 Revised $\frac{T_o}{T_p}$ (21.59)

Family #1

$$\left. \begin{array}{l} \frac{T_o}{T_p} = 6.17 \\ \frac{T_o}{T_p} = 6 \end{array} \right\}$$

$$\frac{T_o}{T_p} = 6$$

$$9 \text{ Revised } T_p = \frac{T_o}{\frac{T_o}{T_p} \text{ Rev.}} = \frac{5.7}{6} = 0.95$$

10 Compute q_p

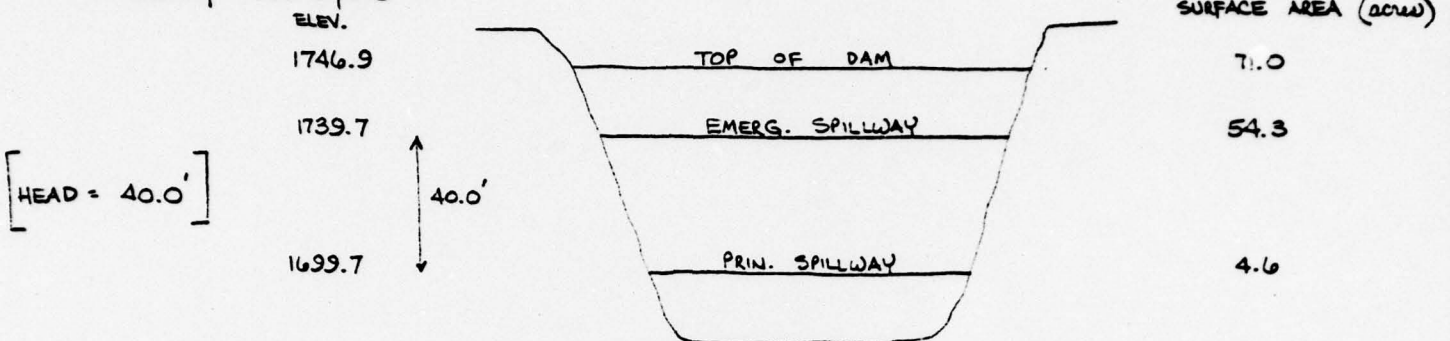
$$q_p = \frac{484 A}{\text{Rev. } T_p} = \frac{484 \times 3.6}{0.95} = 1834 \text{ cfs.}$$

11 Compute Q_{9p}

$$Q_{9p} = Q \times q_p = 20.3 \times 1834 = 37230 \text{ cfs}$$

A in Sq. Miles

SPILLWAY ANALYSIS:



Reservoir Detention Volume (RDV):

$$RDV = A \times h = \left(\frac{54.3 + 4.6}{2} \right) (40.0) = 1178.0 \text{ AF}$$

Inflow Runoff Volume (IRV):

$$IRV = \frac{Q}{12} \times A_{22} = \frac{30.3}{12} \times 2304 = 3897.6 \text{ AF}$$

Ratio: $\frac{RDV}{IRV} = \frac{1178}{3897.6} = .302$

Ratio: $\frac{OPR}{IPR} = .86$

$$OPR = (.86) IPR = (.86)(18503) = 15913 \text{ cfs} \quad [\text{OUTFLOW PEAK RATE}]$$

(USE 15900 cfs)

#191C - 381B

SPILLWAY DISCHARGES :

[PMF]

$$\text{PEAK OUTFLOW} = 15913 \text{ cfs}$$

$$\text{PRIN. SPILLWAY} = 125 \text{ cfs} \quad (\text{W.S. ELEV.} = \text{CREST EMERG. SPILLWAY})$$

$$\text{REQ'D IN 2 EMERG. SPILLWAYS} = 15788 \text{ cfs}$$

EMERG. SPILLWAYS : ANALYZE AS BROADCRESTED WEIR

$$Q = CLH^{3/2}$$

$$C = 3.087$$

$$L = 250' = 50' + 200'$$

$$H^{3/2} = \frac{Q}{CL} = \frac{15788}{(3.087)(250)}$$

$$H^{3/2} = 20.457402$$

$$H = 7.5'$$

$$(\text{ACTUAL } H = 7.2')$$

WIDTH	BOTTOM WIDTH	
	EAST	WEST
	TOP	WEST
	93.2	243.2
BOTTOM	50	200
AVE. :	71.6	221.6
	L = 293.2	

$$H^{3/2} = 17.443214$$

$$H = 6.7'$$

$$\text{FREEBOARD} = 0.5'$$

DISCHARGE IN EMERGENCY SPILLWAYS @ MAX. HIGH WATER (7.2' FLOW DEPTH)

$$Q = CLH^{3/2} = (3.087)(293.2)(7.2)^{3/2}$$

[OUTFLOW]

$$Q = 17486 \text{ cfs}$$

$$(\text{USE } 17468 \text{ cfs})$$

#191C - 3813

PRINCIPAL SPILLWAY CAPACITY @ MAX. HIGH WATER :

(30" CONDUIT - FLOW CONTROL)

ELEV. — TOP OF DAM 1746.9

PIPE OUTLET 1677.0

HEAD = 69.9'

(ORIFICE ; FULL FLOW)

$$Q = A \sqrt{\frac{2gH}{1 + K_e + K_b + K_p L}}$$

$$A(30" \text{ PIPE}) = 4.909 \text{ ft}^2$$

$$H = 69.9' \quad L = 326.33'$$

$$K_e = 0.5 \quad K_b = 0.45 \quad K_p = 0.0123$$

$$= 4.909 \sqrt{\frac{2(32.2)(69.9)}{1 + 0.5 + 0.45 + \underbrace{(0.0123)(326.33)}_{4.242}}$$

$$= 4.909 \sqrt{726.9961}$$

$$[\text{OUTFLOW}] \quad Q = 132.4 \text{ cfs}$$

PRINCIPAL SPILLWAY CAPACITY @ W.S. ELEVATION = CREST OF EMERGENCY SPILLWAYS

ELEV. — EMERG. SPILLWAY CREST 1739.7

PIPE OUTLET 1677.0

HEAD = 62.7' (ORIFICE ; FULL FLOW)

$$Q = 4.909 \sqrt{\frac{2(32.2)(62.7)}{1.95 + 4.242}}$$

$$= 4.909 \sqrt{652.1124}$$

$$[\text{OUTFLOW}] \quad Q = 125.4 \text{ cfs}$$

BATAVIA KILL #3

#191C-3818

6

RESERVOIR DRAIN CAPACITY @ W.S. ELEV. = CREST OF PRIN. SPILLWAY

16" ϕ CAST IRON $n = .015$

HEAD = 16.75'

1699.7

$\frac{1682.95}{16.75}$

$A = 1.396 \text{ ft}^2$ $L = 44'$

$K_e = 0.5$

$K_b = .02$

$K_p = .02846$

$$Q = A \sqrt{\frac{2gH}{1 + K_e + K_b + K_p L}}$$

$$= 1.396 \sqrt{\frac{2(32.2)(16.75)}{1 + 0.5 + .02 + \frac{(.02846)(44)}{1.094}}}$$

$$= 1.396 \sqrt{412.66258}$$

$$Q = 28.4 \text{ cfs}$$

[OUTFLOW]

$$\text{BEND} = \frac{2.5}{40} = .0625 = \tan \beta$$

$$\beta = 3.576^\circ = 3^\circ 35'$$

$$K_b = \frac{n \beta}{3} = \frac{(.015)(3.576)}{3} = .018$$

$$K_p = \frac{5100 n^2}{D^{4/3}} = \frac{5100 (.015)^2}{(16)^{4/3}} = .02846$$

MAXIMUM KNOWN FLOOD @ ELEV. = 1709.7

(10' above PRIN. SPILLWAY CREST)

ELEV. — 1709.7

PIPE OUTLET — 1677.0

HEAD — 32.7'

$$Q = 4.909 \sqrt{\frac{2(32.2)(32.7)}{1.95 + 4.242}}$$

$$= 4.909 \sqrt{340.09687}$$

[OUTFLOW] $Q = 90.5 \text{ cfs}$

APPENDIX F

REFERENCES

- 1) U.S. Department of Commerce, Technical Paper No. 40, Rainfall Frequency Atlas of the United States, May 1961.
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- 4) T.W. Lambe and R.V. Whitman, Soil Mechanics, John Wiley and Sons, 1965.
- 5) W.D. Thornbury, Principles of Geomorphology, John Wiley and Sons, 1969.
- 6) University of the State of New York, Geology of New York, Education Leaflet 20, Reprinted 1973.